

# Physics 413: Introduction to Electrodynamics

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Grading:	Test 1	40	points
	Test 2	40	points
	HWs	40	points
	Final	80	points
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			200 points

Exams: Test 1: Wednesday, 2013 Feb. 6  
Test 2: Friday, 2013 March 8

Final: Friday, 2013 March 22, 10:15

Material: Griffiths, Intro to Electrodynamics

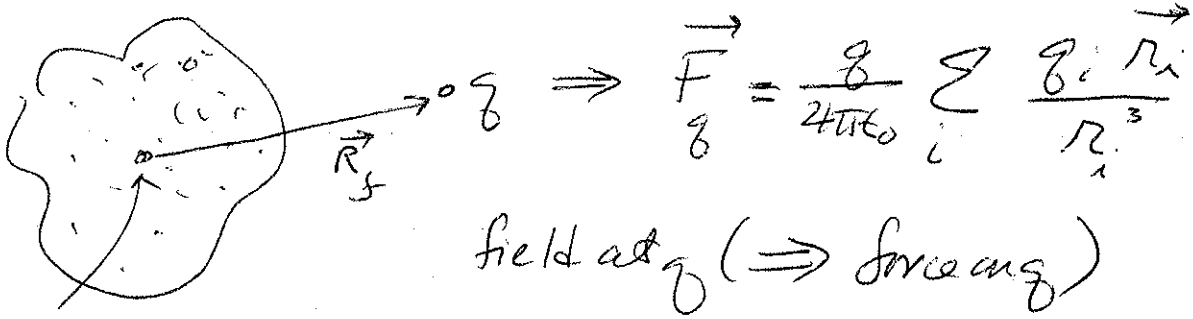
Chapters 5, 6, 7, 8, (9)

# Chapter 5: Magnetostatics

Comment: Not "static", magnetic fields arise from changes in motion  $\Rightarrow$  magnetostatics  $\Rightarrow$  steady currents  $\Rightarrow$  steady fields

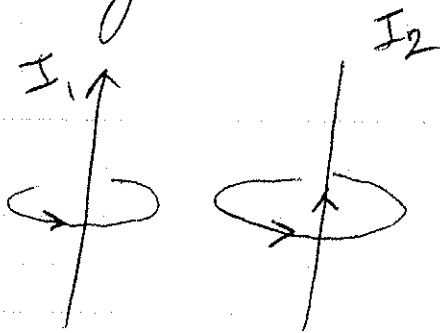
## Goals:

(i) Electrostatics



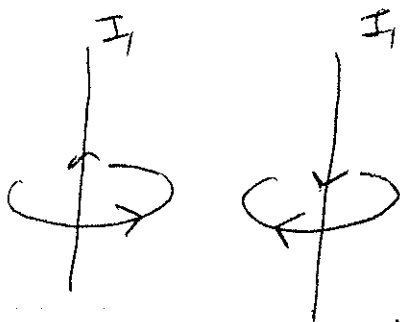
$q_i$

(ii) Magnetostatics



$I_1 \parallel I_2$

$\Rightarrow$  force is attractive,  $I_1, I_2$  pulled together



$I_1$  anti- $\parallel$  to  $I_2$

$\Rightarrow$  force is repulsive,  $I_1, I_2$  repel each other

follows from  $\vec{F}_2 \propto I_2 \hat{n}_2 \times \vec{B}_1$

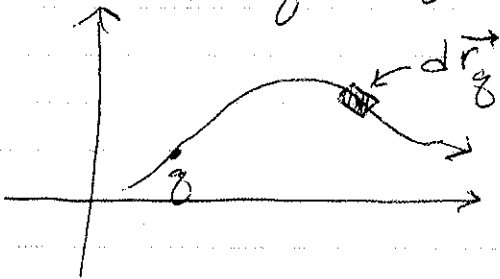
and  $\int \vec{g} \cdot \vec{B}$

for a particle w/ charge  $q$  moving through an EM field,

$$\vec{F} = \underbrace{q\vec{E}}_{\text{Coulomb force}} + \underbrace{q(\vec{v} \times \vec{B})}_{\text{Lorentz force}}$$

Work:

$$\vec{F} \cdot d\vec{r}_q = q\vec{E} \cdot d\vec{r}_q + q(\vec{v} \times \vec{B}) \cdot d\vec{r}_q$$



← region containing  $\vec{E}, \vec{B}$

unless stated otherwise,  $q$  does not affect external  $\vec{E} \& \vec{B}$

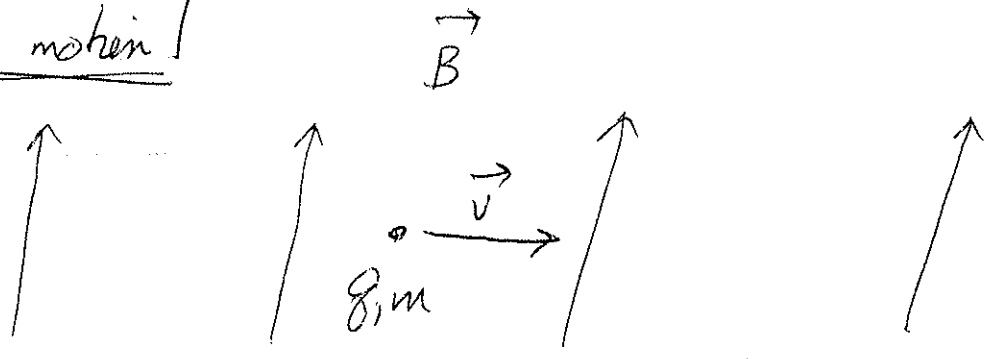
$$\Rightarrow \vec{F} \cdot d\vec{r}_q = q(\vec{E} \cdot d\vec{r}_q) + 0$$

and energy

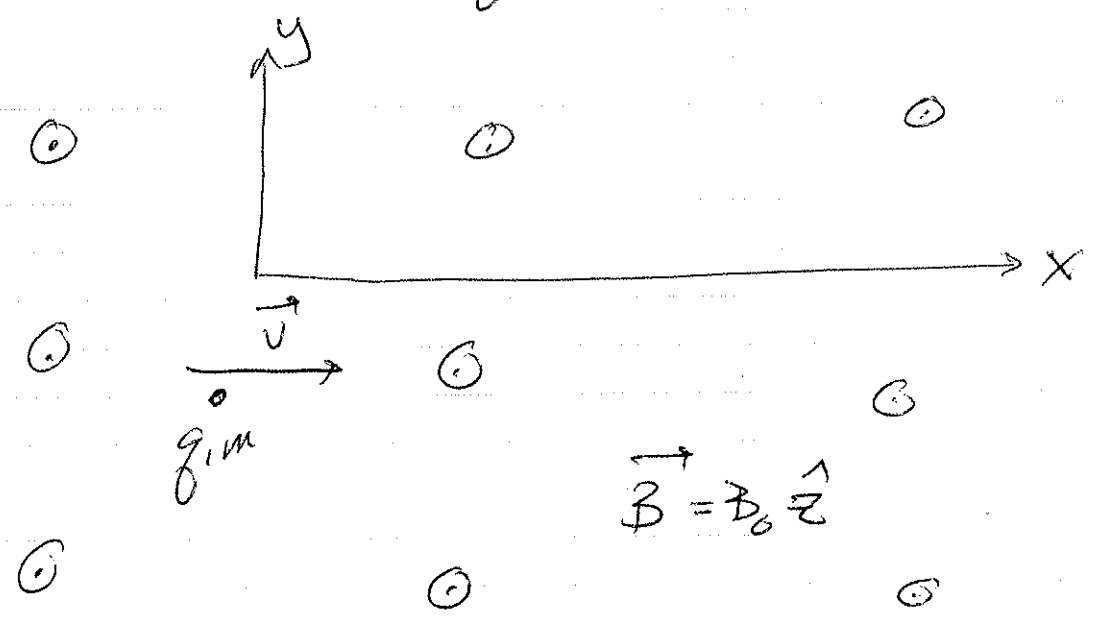
$$\text{Energy}_q = \frac{1}{2}mv^2 + qV$$

note: magnetic field does no work

# Cyclotron motion



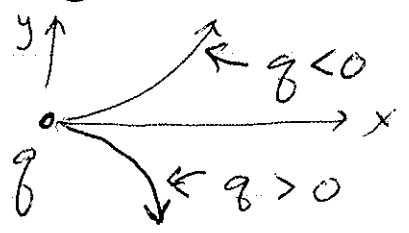
Assume  $\vec{E} = 0 \Rightarrow \vec{F} = q(\vec{v} \times \vec{B})$ , Lorentz force -  
 sky (a)



$$\Rightarrow \vec{F} = q(\vec{v} \times \vec{B})$$

$$= q(v_y B_z - v_z B_y, v_z B_x - v_x B_z, v_x B_y - v_y B_x)$$

$F_y = -qv_x B_z$ 
 $F_z = 0 \Rightarrow$  motion in 2D



Solve:

$$\left\{ \begin{aligned} F_x &= m\ddot{x} = qv_y B_z \\ F_y &= m\ddot{y} = -qv_x B_z \\ F_z &= m\ddot{z} = 0 \implies \dot{z} = v_z(0) \implies z = v_z(0)t + z(0) \end{aligned} \right. \left\{ \begin{array}{l} \text{subject to } t=0, \\ \vec{r}_0 = 0, \vec{v} = v_0 \hat{x} \\ \text{initial conditions} \end{array} \right.$$

drifts upward in z,  
if initial velocity has  
a z-component  
⇒ fraustration

Consider xy motion

$$\left\{ \begin{aligned} m\ddot{x} &= q\dot{y} B_z \quad \leftarrow \text{from } \vec{B} = B_0 \hat{z} \\ m\ddot{y} &= -q\dot{x} B_z \quad \searrow \end{aligned} \right. \begin{matrix} \text{(a)} \\ \text{(b)} \end{matrix}$$

divide by m and define the cyclotron frequencies,

$$\boxed{\omega_c = \left| \frac{qB_0}{m} \right|}$$

Strategy

a) Integrate

$$\left. \begin{aligned} \ddot{x} = \dot{y}\omega_c &\implies \dot{x} = \dot{x}_0 + \omega_c(y - y_0) \\ \ddot{y} = -\dot{x}\omega_c &\implies \dot{y} = \dot{y}_0 - \omega_c(x - x_0) \end{aligned} \right\}$$

b) replace  $\dot{y}$  in (a)

$$\ddot{x} = \omega_c \left[ -x\omega_c \right]$$

(6)

$$\Rightarrow \ddot{x} + \omega_c^2 x = 0$$

$$\omega_c \text{ is real } \Rightarrow \boxed{x(t) = A \cos \omega_c t + B \sin \omega_c t}$$

$$\Rightarrow \boxed{\dot{x}(t) = -\omega_c A \sin \omega_c t + \omega_c B \cos \omega_c t}$$

$$\text{at } t=0 \Rightarrow x(0) = 0, \dot{x}(0) = v_0$$

$$\text{and so, } A = 0, B = \frac{v_0}{\omega_c}$$

$$\text{Sol}^n \text{ subject to ICs is } \boxed{x(t) = \frac{v_0}{\omega_c} \sin \omega_c t}$$

(c) replace  $\dot{x}$  in  $\dot{y}$  [(b)]

$$\dot{y} = -\omega_c \left[ v_0 + \omega_c y \right]$$

$$\ddot{y} + \omega_c^2 y = -\omega_c v_0$$

Can solve this by considering homogeneous sol<sup>n</sup> and particular solution or ...

$$\ddot{y} + \omega_c^2 \left( y + \frac{v_0}{\omega_c} \right) = 0$$

$$\ddot{u} + \omega_c^2 u = 0 \Rightarrow u = C \cos \omega_c t + D \sin \omega_c t$$

$$y(t) = C \cos \omega_c t + D \sin \omega_c t - \frac{v_0}{\omega_c}$$

(7)

$$y(t) = C \cos \omega_c t + D \sin \omega_c t + (V_0 / \omega_c)$$

$$\dot{y}(t) = -\omega_c C \sin \omega_c t + \omega_c D \cos \omega_c t$$

ICs ( $y(0) = \dot{y}(0) = 0$ )  $\Rightarrow D = 0$  &  $C = \frac{V_0}{\omega_c}$

and  $y$  sol<sup>n</sup> is

$$y(t) = \frac{V_0}{\omega_c} \cos \omega_c t - \frac{V_0}{\omega_c}$$

So, we have

$$x(t) = \frac{V_0}{\omega_c} \sin(\omega_c t)$$

$$y(t) = \frac{V_0}{\omega_c} \cos(\omega_c t) - \frac{V_0}{\omega_c}$$

perfectly fine, but, let us manipulate sol<sup>n</sup>.

$$r_g^2 = x^2 + \cancel{y^2} = \left(\frac{V_0}{\omega_c}\right)^2 \left[\sin^2 \omega_c t + \cos^2 \omega_c t\right] = \left(\frac{V_0}{\omega_c}\right)^2$$

$$\left(y(t) + \frac{V_0}{\omega_c}\right)^2$$

motion is circular w/ radius

$$r_g = \text{gyro radius} = \frac{V_0}{\omega_c} = \frac{m v_{\perp}}{q B}$$

$\omega$  / frequency

$$\omega_c = \frac{q B}{m} \text{ , cyclotron frequency}$$

## Typical #'s

Examples:

$$\omega_c = \frac{qB}{m}$$

$$R = \frac{mV_{\perp}}{qB}$$

In most situations, electrons are much more mobile than ions and we look at cyclotron motion of  $e^{-}$ 's.

$$\omega_{\text{cyc}} = \frac{1.6 \times 10^{-19} \text{ B}}{9.1 \times 10^{-31} \text{ kg}} = 1.8 \times 10^{11} \text{ B s}^{-1} \quad \equiv \text{cyclotron frequency}$$

$$R = \frac{9.1 \times 10^{-31} \text{ kg } V_{\perp}}{1.6 \times 10^{-19} \text{ C } B} = 5.7 \times 10^{-12} \frac{V_{\perp}}{B} \text{ m} \quad \equiv \text{gyro radius}$$

## N\*'s (Pulsars)

$$B_* \approx 10^{13} \text{ G} = 10^9 \text{ T}, \quad V_{\perp} \approx 7 \times 10^7 \frac{\text{m}}{\text{s}} \quad (T \approx 10^8 \text{ K}) \rightarrow 7 \text{ keV}$$

$$\Rightarrow \begin{cases} \omega_{\text{cyc}} \approx 1.8 \times 10^{20} \text{ s}^{-1} \Rightarrow \text{X-rays} \approx 100 \text{ keV} \\ R \approx 4 \times 10^{-13} \text{ m} \approx 400 \text{ a}_{\text{nucleon}} \end{cases}$$

comment:  $\hbar \omega_{\text{cyc}} \gg \hbar T_e \Rightarrow$  low energy gas and motion is quantized  $m \perp \text{dir}^n$   
 $E_{\perp} = n \hbar \omega_{\text{cyc}}$

## Sun (flare)

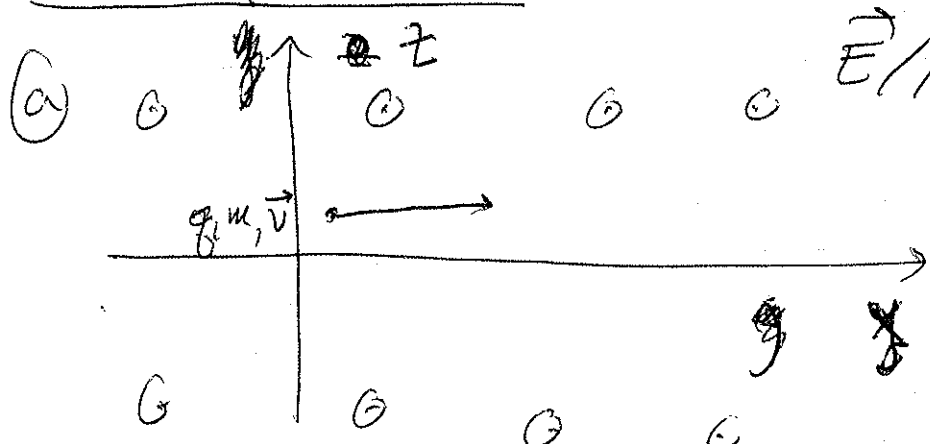
$$B_* \approx 10^3 \text{ G} \approx 0.1 \text{ T}, \quad V_{\perp} \approx 7 \times 10^7 \frac{\text{m}}{\text{s}}$$

$$\Rightarrow \begin{cases} \omega_{\text{cyc}} \approx 1.8 \times 10^{10} \text{ s}^{-1} \Rightarrow \text{microwaves} \\ R \approx 4 \times 10^{-3} \text{ m} \end{cases}$$

$\hbar \omega_{\text{cyc}} \ll \hbar T \Rightarrow$  "classical" motion



Consider effects of  $\vec{E}$

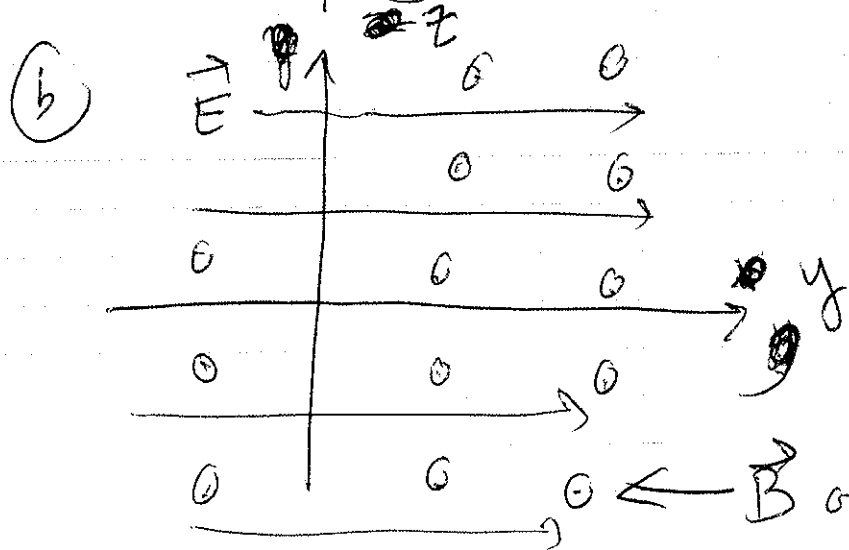


$\vec{E} // \hat{z}, \vec{E} = E_0 \hat{z}, \vec{B} = B_0 \hat{x}$

$\vec{F} = q\vec{E} + q(\vec{v} \times \vec{B})$  2D circular motion in y-z plane

↳ uniform acceleration in  $\hat{x}$  direction

⇒ "Opening" helical motion



Crossed  $\vec{E} \perp \vec{B}$   
 $\vec{B} = B_0 \hat{x}, \vec{E} = E_0 \hat{z}$

←  $\vec{B}$  out of paper

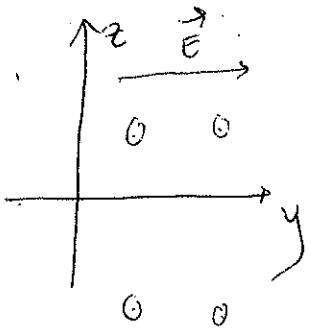
Lorentz force ⇒ circular motion projected onto  $y-z$  plane

Calculus free ⇒ force has bites to right (or left) but motion can be calculated

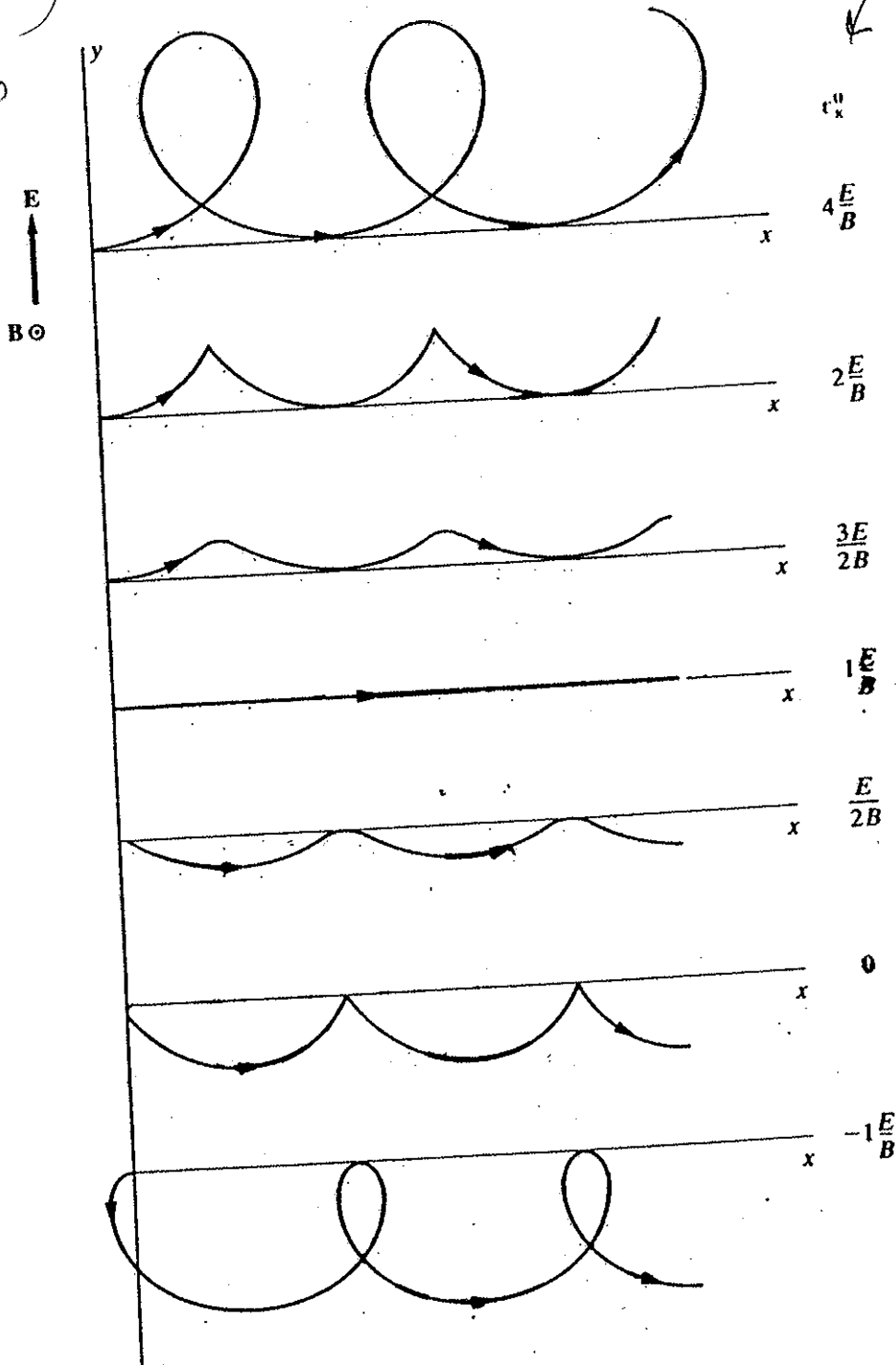
drawn for an  $e^-$

$v_y^0 = 0$   
 $v_x^0$

recall that my  
coordinate  
system was



$\vec{B}$   
 $\Rightarrow$  drift is in  
 $-z$  direction



**FIGURE 1-4** Trajectories in the  $xy$  plane of a charged particle in crossed  $E$ , and  $B_z$  fields for various initial velocities along the  $x$  axis

Generalize from point charge  $q$  to current distributions

Consider magnetic forces on currents

$$\vec{F} = q (\vec{E} + \vec{v} \times \vec{B})$$

for a collection of charges

$$= \sum q_i (\vec{E}_m(\vec{r}_i) + \vec{v}_i \times \vec{B}_m(\vec{r}_i))$$

↑ microscopic fields

Macroscopic fields are averages of microscopic fields. Cast  $\vec{F}$  into a more reasonable form. For example,

$$\vec{E}_m(\vec{r}) = \vec{E}_M(\vec{r}) + \delta \vec{E}$$

↑ macroscopic field

↙ fluctuates about  $\vec{E}_M(\vec{r})$

and so, the force on a volume element  $\Delta V$  is  $\Delta \vec{F}$

$$\begin{aligned} \Delta \vec{F} &= \int_{\Delta V} (\rho_M + \delta \rho) [\vec{E}_M + \delta \vec{E}] dV \\ &\quad + \int_{\Delta V} (\vec{J}_M + \delta \vec{J}) \times (\vec{B}_M + \delta \vec{B}) dV \\ &= \int [\rho_M \vec{E}_M + \rho_M \delta \vec{E} + \delta \rho \vec{E}_M + \delta \rho \delta \vec{E}] dV \\ &\quad + \int [\vec{J}_M \times \vec{B}_M + \vec{J}_M \times \delta \vec{B} + \delta \vec{J} \times \vec{B}_M + \delta \vec{J} \times \delta \vec{B}] dV \end{aligned}$$

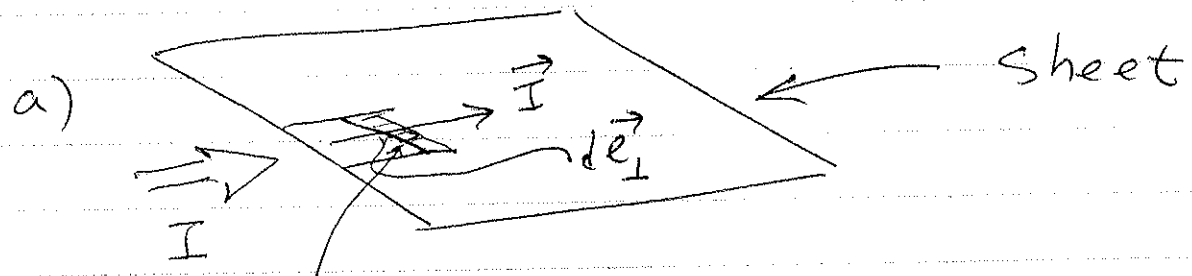
all 1<sup>st</sup> order terms integrate (average) to 0. ← can be important

$$= \underbrace{\int [\rho_M \vec{E}_M + \vec{J}_M \times \vec{B}_M] dV}_{\text{macroscopic fields}} + \underbrace{\int [\delta \rho \delta \vec{E} + \delta \vec{J} \times \delta \vec{B}] dV}_{\text{fluctuation forces}}$$

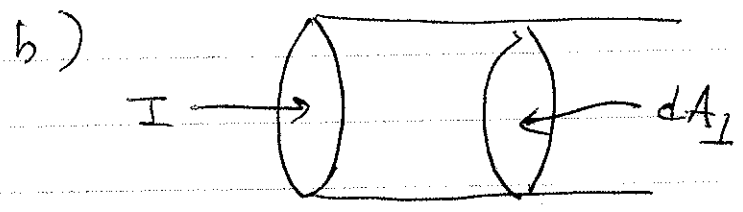
fluctuation forces (in a wire driven by a battery  $\vec{F} = 0$ )  
("resistance" → Ohmic losses)

# Current Distributions

Defn:



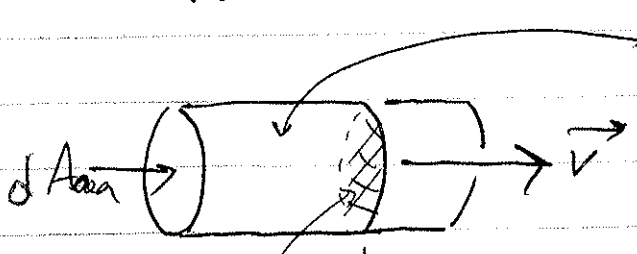
$$\vec{K} = \frac{d\vec{I}}{dA_1} \rightarrow d\vec{I} = \vec{K} dA_1$$



$$\vec{J} = \frac{d\vec{I}}{dA_1} \rightarrow d\vec{I} = \vec{J} dA_1$$

[current density] is a current flux.

c) Suppose I have a volume of charge which moves?



$\rho =$  charge density

Surface  $h = v dt =$  length of cylinder which crosses surface

$$\rightarrow \left( \frac{\text{Charge which crosses surface}}{\text{second}} \right) = \frac{\rho (dA h)}{dt} = \frac{\rho dA v dt}{dt}$$

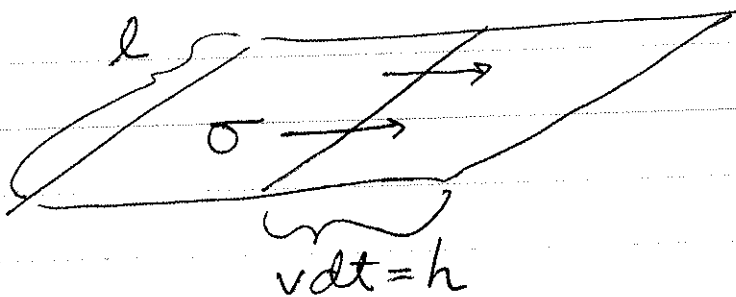
In terms of  $\vec{J}$ , what law we define?

$$dI = J dA$$

$$\rightarrow J dA = \rho dA v \rightarrow J = \rho v \left[ \frac{C}{L^2-t} \right]$$

In general,  $\boxed{\vec{J} = \rho \vec{v}}$

d) Suppose I has a surface charge



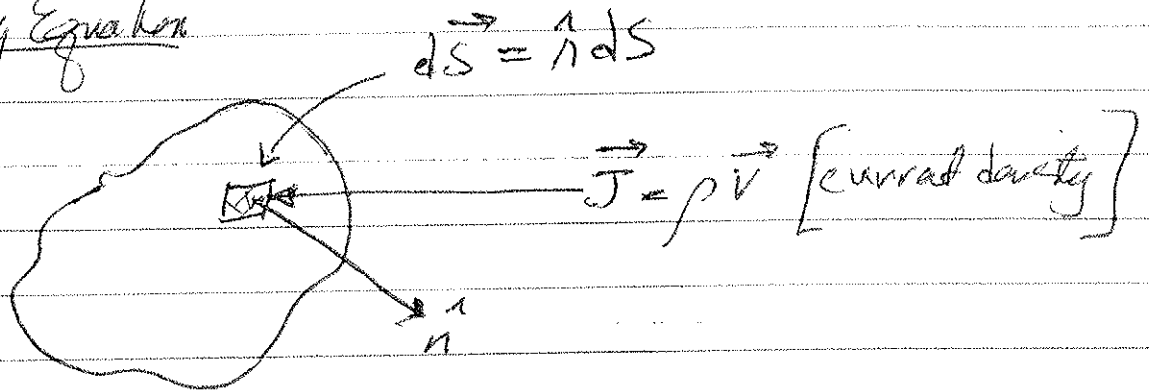
$$I = \underbrace{\sigma l h}_{\text{charge}} \frac{1}{dt} = \frac{\sigma l v db}{dt}$$
$$= \sigma l v$$

again,  $K = \frac{I}{l} = \sigma v$

In general,  $\vec{K} = \sigma \vec{v}$

# Continuity Equation

(a)



We then have

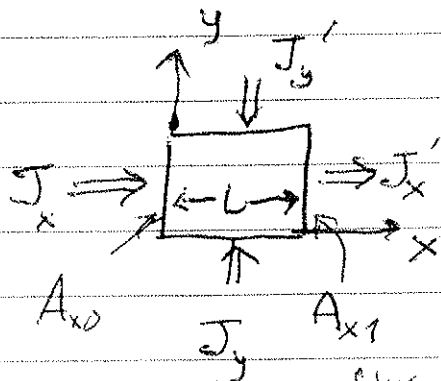
$$\oint \vec{J} \cdot d\vec{S} \equiv \left. \begin{array}{l} \text{Integral of flux over} \\ \text{surface of volume} \end{array} \right\} \begin{array}{l} \text{[charge/time]} \\ \text{change in} \\ \text{charge contained} \\ \text{in volume} \\ \text{per time} \end{array}$$

$$= \frac{d}{dt} \int \rho d^3x$$

$$\Rightarrow \int (\nabla \cdot \vec{J}) d^3x = \frac{d}{dt} \int \rho d^3x$$

$$\text{or } \boxed{\nabla \cdot \vec{J} + \frac{\partial \rho}{\partial t} = 0}$$

(b)



Consider 2D flow for simplicity

$$(a) \left[ \overbrace{\rho_0 v_{x0}}^{\text{flux}} \times A_{x0} - \overbrace{\rho_1 v_{x1}}^{\text{flux}} \times A_{x1} \right] \times \Delta t = \Delta Q$$

$$\left[ \rho_0 v_{x0} A_{x0} - \left( \rho_0 v_{x0} A_{x0} + L \frac{\partial}{\partial x} \left\{ \rho v_x A_x \right\} \right) \right] \Delta t = \Delta Q$$

$$-L \frac{\partial}{\partial x} \{ \rho v_x A_x \} \Delta t = \Delta Q$$

divide by the volume of the box,  $(L A_x) \Delta(\text{density})$

$$-\frac{1}{A_x} \frac{\partial}{\partial x} \{ \rho v_x A_x \} \Delta t = \frac{\Delta Q}{\text{Volume}} = \left( \frac{\Delta Q}{L A_x} \right) = \Delta p$$

$$\Rightarrow \frac{\Delta p}{\Delta t} + \frac{\partial}{\partial x} (\rho v_x A_x) \frac{1}{A_x} = 0$$

$$\text{as } \Delta t \rightarrow 0 \rightarrow \frac{\partial p}{\partial t} + \frac{1}{A_x} \frac{\partial}{\partial x} (\rho v_x A_x) = 0$$

$\underbrace{\qquad\qquad\qquad}_{\vec{\nabla} \cdot \rho \vec{v}}$

$$\boxed{\frac{\partial p}{\partial t} + \vec{\nabla} \cdot \rho \vec{v} = 0}$$

Continuity Equation

# Lorentz force + Coulomb force

For purely macroscopic forces, we have

$$(i) \vec{F} = (q \vec{E} + q(\vec{v} \times \vec{B}))$$

$$(ii) d\vec{F} = (\lambda dr \vec{E} + I dr \vec{r} \times \vec{B})$$

$$(iii) d\vec{F} = (\sigma \vec{E} + \vec{K} \times \vec{B}) dS$$

$$(iii) d\vec{F} = (\rho \vec{E} + \vec{J} \times \vec{B}) dV$$

"point"

"line"

"surface"

"volume"

Examples,

A) Ignore gravity

loop sits in zy-plane

$$a) \vec{F} = \oint I d\vec{r} \times \vec{B}$$

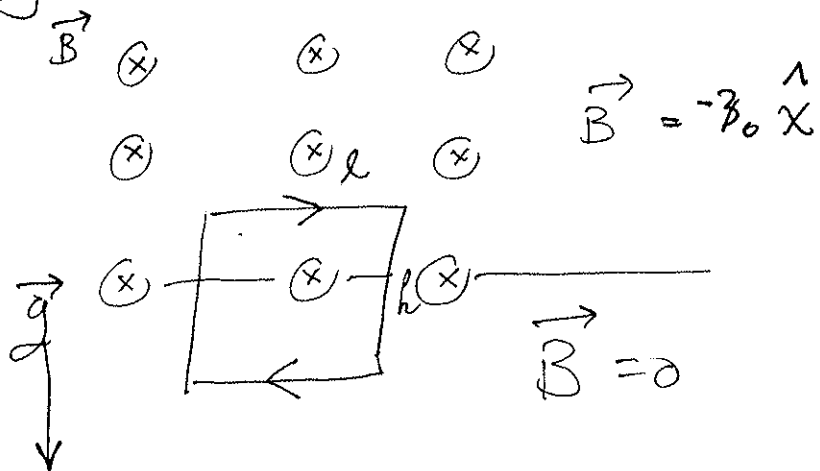
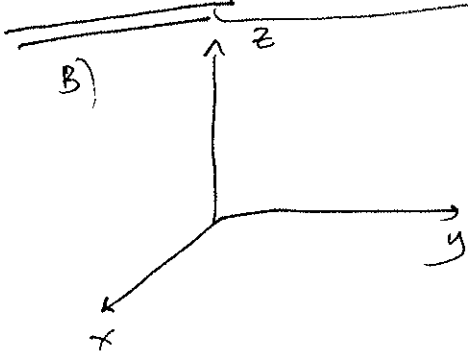
$$= I l \hat{x} B_0 + 0 + I l (-\hat{x}) B_0 + 0$$

$$= 0$$

⇒ no translational force, however,

$$b) \vec{N} = \left[ \frac{R}{2} I l + \frac{R}{2} I l \right] \hat{y} B_0 = I h l y^1 B_0$$

⇒ rotate about y-axis so that loop sits in xy-plane



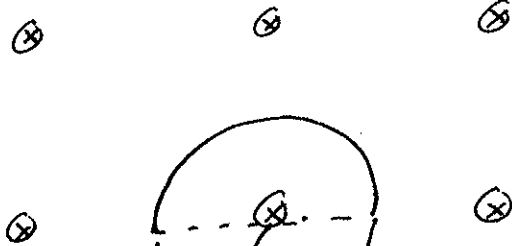


To make loop "float", I must be in CW direction

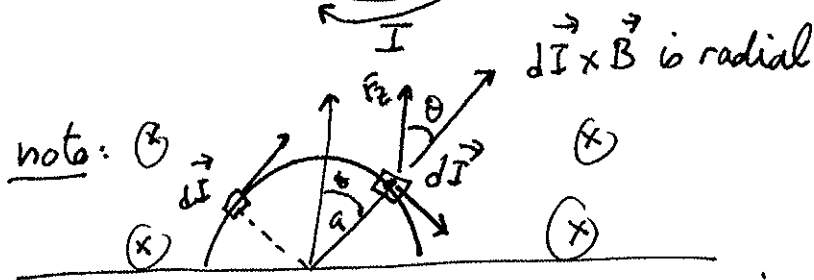
$$\vec{F}_B = IB\hat{z}l + \underbrace{IB\frac{a}{2}\hat{y} + 0 + IB\frac{a}{2}(\hat{y})}_{\rightarrow 0}$$

$$\vec{F}_B + \vec{F}_g = IB\hat{z}l - mg\hat{z} = 0 \rightarrow I = \frac{mg}{Bl}$$

c)



Q: What I is needed to make half of the circle "float" into the field region?



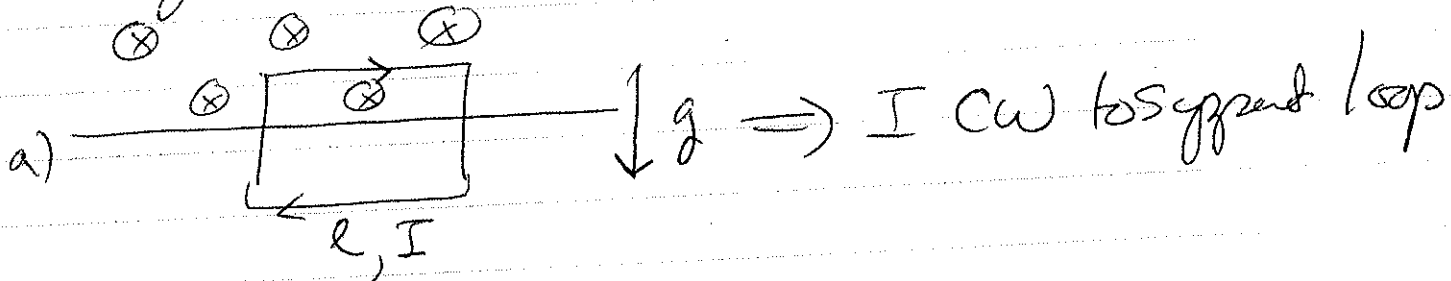
By symmetry we need only consider  $F_z$ .

$$dF_z = [I a d\theta B] \cos\theta$$

$$F_{z, total} = 2IaB \int_0^{\pi/2} \cos\theta d\theta = 2aIB$$

$$\Rightarrow F_{z, total} + F_g = 0 \Rightarrow 2aIB - mg = 0 \Rightarrow I = \frac{mg}{2aB}$$

# Magnetic "Work" ← what is the meaning of this?



a) 
$$\vec{F}_B = I \vec{dl} \times \vec{B} = I l B \hat{z}$$

$$\vec{F}_g = -Mg \hat{z}$$
} 
$$I = \frac{Mg}{lB}$$

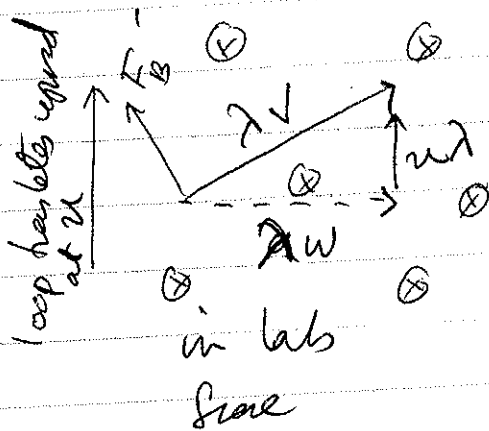
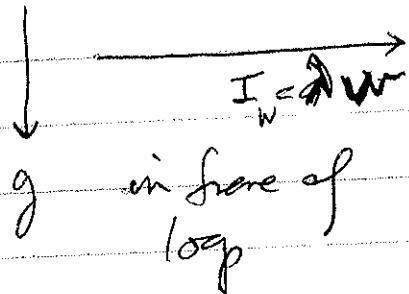
b) If  $I \uparrow \Rightarrow F_B \uparrow \Rightarrow$  loop rises

$$\text{Work} = -\vec{F}_g \cdot d\vec{h} = \vec{F}_g \cdot d\vec{z} = Mgh$$

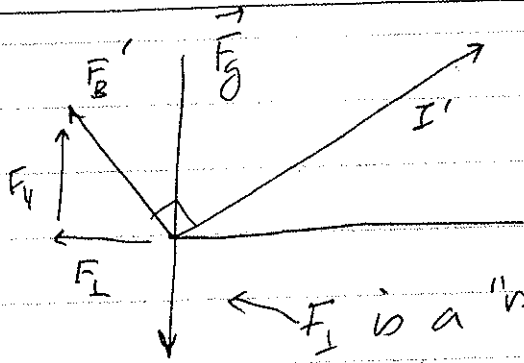
what if  $-\vec{F}_B \cdot d\vec{h}$ ?

$$\rightarrow W = + I l B h$$

Are these both right? Well, yes, but also not the work?



$F_B$  is not // (or anti-//) to  $\vec{g}$



$F_L$  is a "retarding" force which opposes  $I'$   
 $\Rightarrow$  a "battery" needs to push the charges

Energy?

$$(i) F_L = \int I d\vec{r} \times \vec{B} = \int \lambda u B dr_1$$

$$= \lambda u B l$$

$$F_L = I \left( \frac{u}{w} \right) B l$$

we define  $I$  as

$$I = \lambda w$$

$$(ii) W = \int I \left( \frac{u}{w} \right) B l \times dl'$$

$\downarrow$  distance charge travels in time  $dt$  along the  $I$ -direction

$$dl' = w dt$$

$$= \int I \left( \frac{u}{w} \right) B l \times w dt$$

$$= I B l u \int dt$$

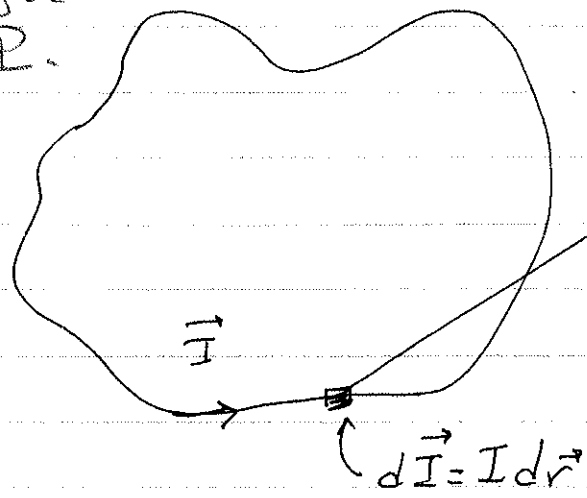
$$W = I B l u h \quad \checkmark$$

# Field Produced by a Current

Biot-Savart law

Biot-Savart law

field of a current loop at some point, P.

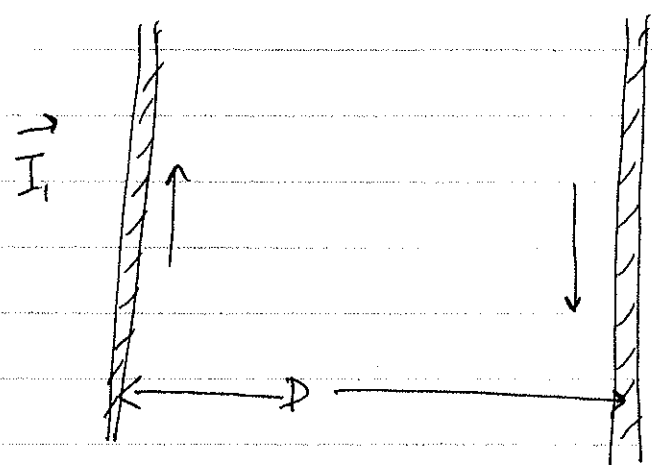


$$d\vec{B} = \frac{\mu_0}{4\pi} \left[ \frac{I d\vec{r} \times \hat{r}}{r^2} \right]$$

where  $\mu_0 \equiv$  permeability of free space  
 $= 4\pi \times 10^{-7} \frac{N}{A^2}$

$$\vec{B} = \frac{\mu_0}{4\pi} \begin{cases} \oint \frac{I d\vec{r} \times \hat{r}}{r^2} & \text{"line"} \\ \int \frac{\vec{K} \times \hat{r}}{r^2} dS & \text{sheet} \\ \int \frac{\vec{J} \times \hat{r}}{r^2} dz & \text{volume} \end{cases}$$

Example, find force on  $\vec{I}_2$  (Return to case of 2 wires)

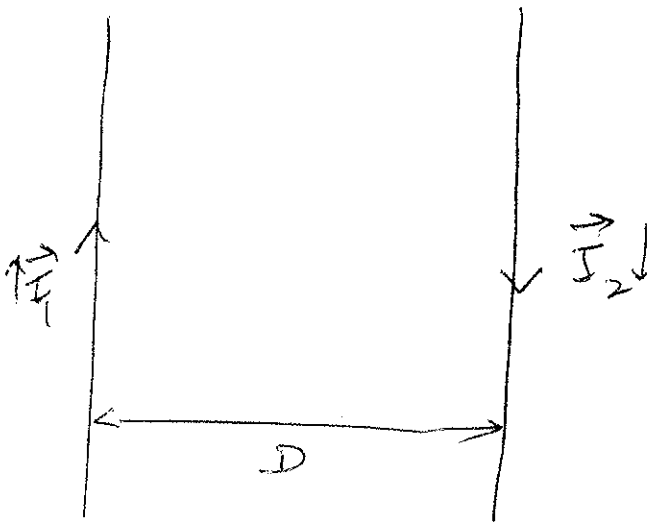


Sol<sup>n</sup>

Find,

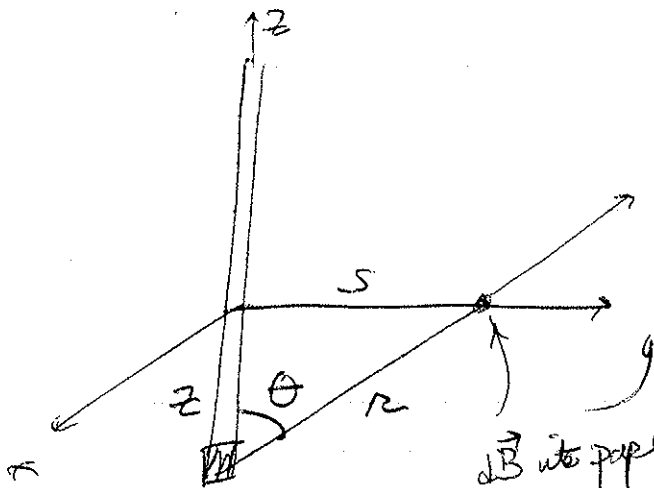
$$\vec{F}_2 = \int I_2 d\vec{r} \times \vec{B}_1$$

→ we need  $\vec{B}_1$



Find the force on wire 2 as a result of  $\vec{B}$  from wire 1

look at 1 wire

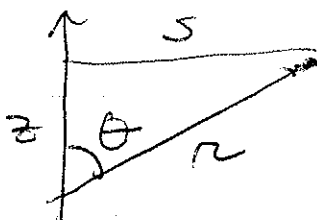


$$d\vec{B} = \frac{\mu_0}{4\pi} \frac{I dz \times \vec{r}}{r^3}$$

$d\vec{B}$  into paper w/ magnitude  $\frac{\mu_0 I r}{r^2} \sin\theta$  from curl

$$\Rightarrow \vec{B} = \frac{\mu_0 I}{4\pi} \hat{z} \int \frac{dz \sin\theta}{(z^2 + s^2)}$$

relate  $\theta$  to  $z$



$$\cos\theta = \frac{z}{r} \quad \& \quad \sin\theta = \frac{s}{r}$$

$$-\sin\theta d\theta = \left[ \frac{dz}{r} - \frac{\frac{1}{2} dz^2 z}{(z^2 + s^2)^2} \right]$$

~~$$= \frac{\mu_0 I s \sin\theta}{4\pi s^2} \int \frac{dz}{r} - \frac{\mu_0 I s \sin\theta}{4\pi s^2} \int \frac{dz^2 z}{(z^2 + s^2)^2}$$~~

$$- \sin \theta d\theta = \left[ \frac{\sin \theta}{s} - \cos^2 \theta \frac{\sin^2 \theta}{s^2} \right] dz$$

$$= \frac{\sin \theta}{s} dz [1 - \cos^2 \theta]$$

$$- \sin \theta d\theta = \frac{\sin^3 \theta}{s} dz [\sin^2 \theta]$$

$$\Rightarrow dz = - \frac{s}{\sin^2 \theta} d\theta$$

and the integral becomes

$$\vec{B} = \frac{\mu_0 I}{4\pi} \hat{\phi} \int_0^\pi \frac{s d\theta}{\sin^2 \theta} \sin^3 \theta \frac{\sin^2 \theta}{s^2}$$

$$= - \frac{\mu_0 I}{4\pi} \hat{\phi} \int_0^\pi \frac{1}{s} \sin \theta d\theta$$

$$= - \frac{\mu_0 I}{4\pi s} \hat{\phi} \left[ \cos \theta \right]_0^\pi$$

$$\vec{B} = \frac{\mu_0 I}{2\pi s} \hat{\phi}$$

The force is then

$$d\vec{F}_2 = \ominus I_2 d\vec{z} \times \vec{B}_1 = -I_2 d\vec{z} \times \left( \frac{\mu_0 I_1}{2\pi D} \hat{\phi} \right)$$

↑  
current is ↓

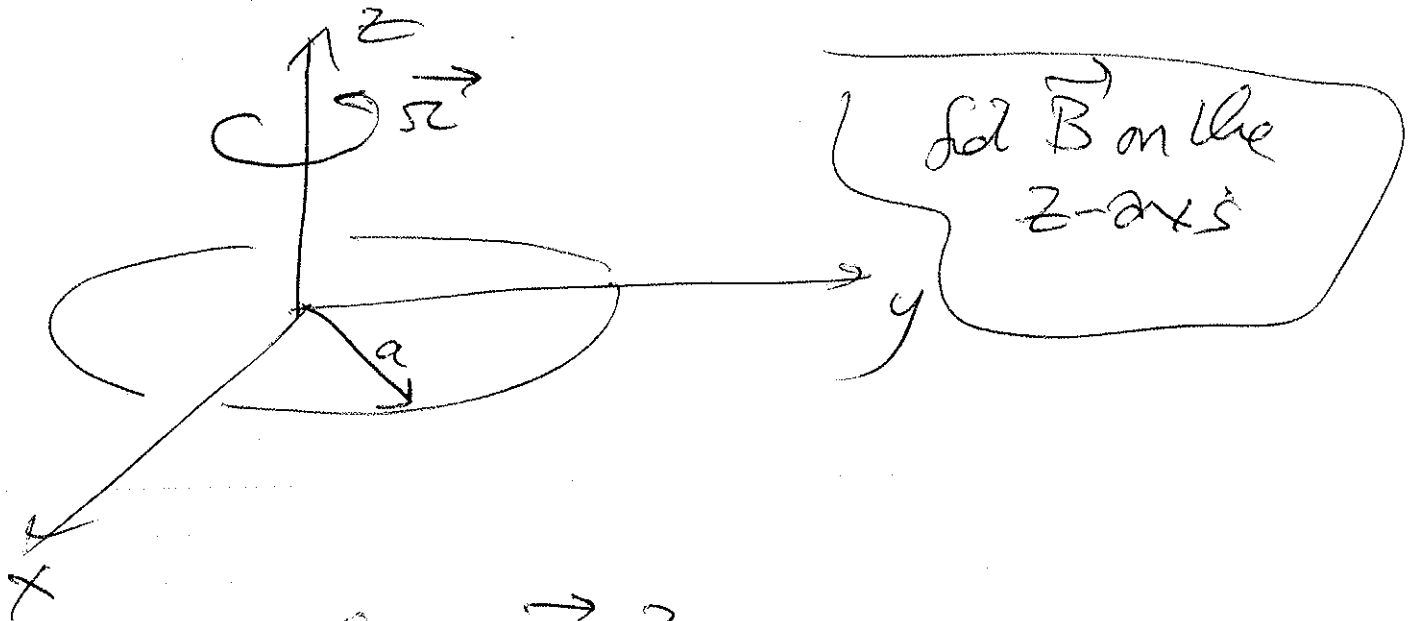
$$= I_2 \frac{\mu_0 I_1}{2\pi D} dz$$

negative

$$\vec{F}_2 = \frac{\mu_0 I_1 I_2 l}{2\pi D} \int dz$$

$$\frac{F_2}{\Delta z} = \frac{\mu_0 I_1 I_2}{2\pi D} \quad ; \text{ force per unit length, } \Delta z$$

Carson "photograph" read  $\mu/\sigma = \frac{Q}{\pi a^2}$



Q: what is  $\vec{K}$ ?

A:  $\vec{K} = \sigma \vec{v}$

Physics 411 (Aethel Medaues)

Q: what is  $\vec{v}$ ?

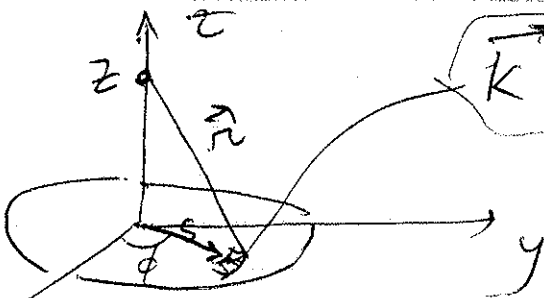
A:  $\vec{v} = \frac{d}{dt}(\hat{i}x + \hat{j}y + \hat{k}z)$

in a disc that rotates at frequency  $\vec{\omega}$ , we had

$$\vec{v} = \vec{\omega} \times \vec{r}$$

$$\Rightarrow \vec{K} = \sigma (\vec{\omega} \times \vec{r}) = \sigma \omega r \hat{\phi}$$

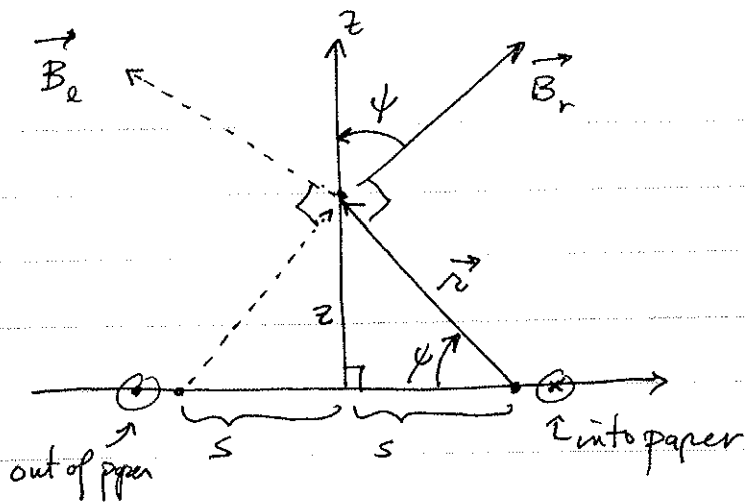
a)  $\text{sol } \vec{B}$



$$\vec{K} dS = \vec{K} r d\phi ds$$

$$d\vec{B} = \frac{\mu_0}{4\pi} \frac{\vec{K} dS \times \vec{r}}{r^2}$$





⇒ By symmetry,  
 $\vec{B}_\perp = 0$ ,  $\perp$  to z-axis

∴ Only need  $B_z$

$$dB_z = \frac{\mu_0}{4\pi} \frac{K ds \times \hat{r}}{r^2} \cos\psi$$

1 since  $\vec{K} \perp \hat{r}$

$$= \frac{\mu_0 \sigma \Omega s^2}{4\pi r^3} \sin\theta ds$$

$$B_z = \frac{\mu_0 \sigma \Omega}{4\pi} \int \frac{s^2}{(s^2+z^2)^{3/2}} ds d\phi$$

$$= \frac{\mu_0 \sigma \Omega}{2} \int \frac{s^3 ds}{(s^2+z^2)^{3/2}}$$

let  $W = s^2 + z^2 \Rightarrow dW = 2s ds$  and  $s^2 = (W - z^2)$

$$B_z = \frac{\mu_0 \sigma \Omega}{2} \int \frac{1}{2} \frac{dW}{W^{3/2}} (W - z^2)$$

$$= \frac{\mu_0 \sigma \Omega}{4} \int \frac{(W - z^2) dW}{W^{3/2}}$$

$$= \frac{\mu_0 \sigma \Omega}{2} \left[ \sqrt{a^2+z^2} - \sqrt{z^2} + \frac{z^2}{\sqrt{a^2+z^2}} - \frac{z^2}{\sqrt{z^2}} \right]$$

$z > 0$

$$B_z = \frac{\mu_0 \sigma \Omega}{2} \left[ \frac{a^2 + 2z^2}{\sqrt{a^2 + z^2}} - 2z \right]$$

$z < 0$

$$B_z = \frac{\mu_0 \sigma \Omega}{2} \left[ \frac{a^2 + 2z^2}{\sqrt{a^2 + z^2}} - 2|z| \right]$$

Comment:

$$\Delta B_z = \frac{\mu_0 \sigma \Omega}{2} \left[ \frac{a^2 + z^2}{\sqrt{a^2 + z^2}} - 2z^+ - \frac{a^2 + 2z^2}{\sqrt{a^2 + z^2}} + 2|z| \right]$$

= 0 at a current sheet

So, (at least for this case),  $B_z$  is continuous at a charged sheet (current carrying sheet)

This is to be contrasted to

$$\Delta E_z = \frac{\sigma}{\epsilon_0}$$

at a charged sheet

### A digression on units

In Electricity and Magnetism, we have:

$$\vec{F}_{es} = K_{es} \frac{Q_1 Q_2 \hat{r}}{r^2}$$

and

$$\vec{F}_m = K_m \frac{2I_1 I_2 \hat{D}}{D} \quad (\text{for 2 wires})$$

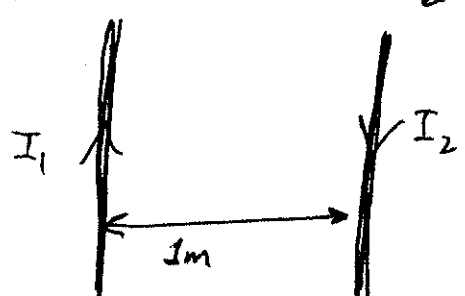
So, there are 2 "new" constants  $K_{es}$  and  $K_m$ ; however, there really is only 1 "new" quantity, the charge.

⇒ can not define  $K_{es}$  and  $K_m$  independently!

The ampere is chosen to be the fourth unit (in addition to meters, kilograms, seconds)

and  $K_m$  is taken to be  $10^{-7}$  using the ampere as a fundamental unit.

or, the ampere is defined as the current which produces a force per unit meter of  $2 \times 10^{-7} \text{ N/m}$  for 2 infinite wires separated by 1m as



the ampere then defines Coulomb (charge)

as

So, given the def<sup>n</sup> of ampere, and

$$|\vec{F}_{es}| = \frac{1}{4\pi\epsilon_0} \frac{Q_1 Q_2}{R^2}$$

$\epsilon_0$  must be adjusted to make the "force" agree w/ expt.

In SI units,  $\epsilon_0 = 8.854 \times 10^{-12} \text{ C}^2/\text{Nm}^2$

≡

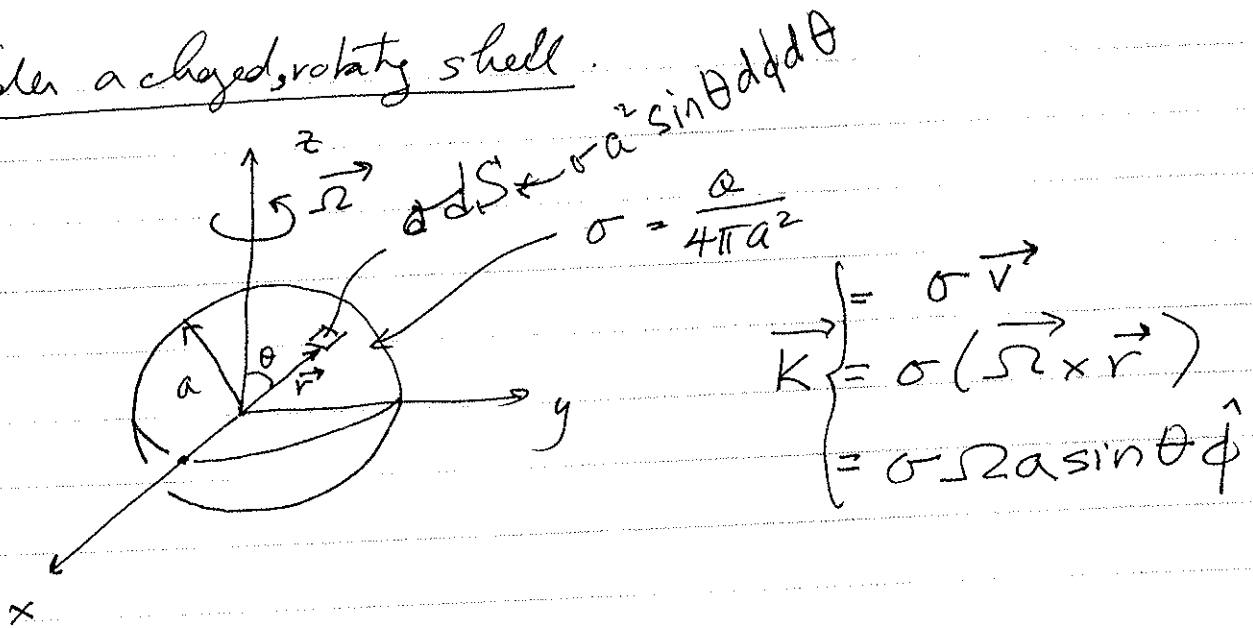
a)  $\frac{K_{es}}{K_m} = \frac{\frac{1}{4\pi\epsilon_0}}{\frac{\mu_0}{4\pi}} = \frac{1}{\epsilon_0 \mu_0} = (\text{const})^2 = c^2$   
Speed of light (in vacuum)

b)  $\vec{F} = I d\vec{r} \times \vec{B}$  or  $[N] = [A][m] \times [B]$   
 $\Rightarrow [B] \equiv \frac{N}{A \cdot m} \equiv \text{Tesla}$

however, (for reasons which are obscure to me),  
but not really

the unit of magnetic field is given in c.g.s. units  
or Gauss =  $10^{-4}$  Tesla

Consider a charged, rotating shell.

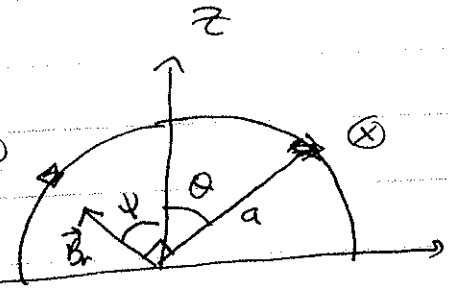


Find  $\vec{B}$  at the center of the shell

By symmetry, we need only

find  $B_z$

$\frac{1}{r^2} \Rightarrow \frac{1}{a^2}$   
 $\frac{1}{r^2} \Rightarrow \frac{1}{a^2} \sin^2 \theta$   
 Projected distance  
 z-axis



$$\Rightarrow dB_z = \frac{\mu_0}{4\pi} \left| \frac{\vec{K} dS \times \hat{r}}{r^2} \right| \underbrace{\cos\left(\frac{\pi}{2} - \theta\right)}_{\cos \psi}$$

and

$$B_z = \frac{\mu_0}{4\pi} \sigma \Omega a \int \sin \theta \frac{1}{a^2} \sin \theta \left[ \sin \theta d\theta d\phi a^2 \right]$$

Area element

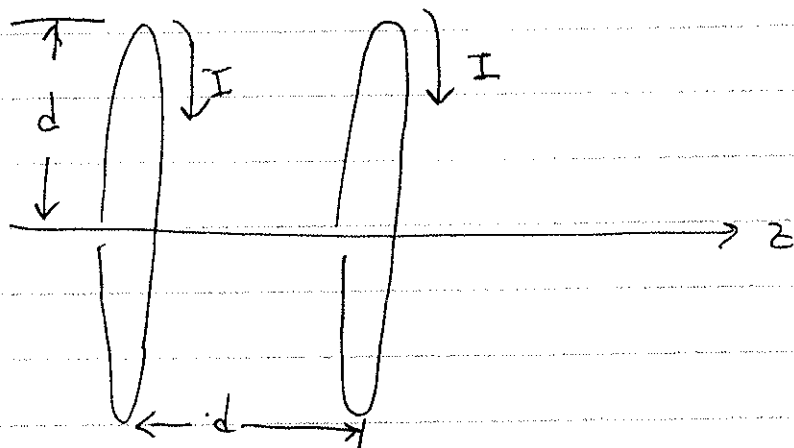
$$= \frac{\mu_0 \sigma \Omega a}{4\pi} \int \sin^2 \theta \sin \theta d\theta d\phi$$

$$= -\frac{\mu_0 \sigma \Omega a}{4\pi} \int (1 - \cos^2 \theta) d(\cos \theta) d\phi$$

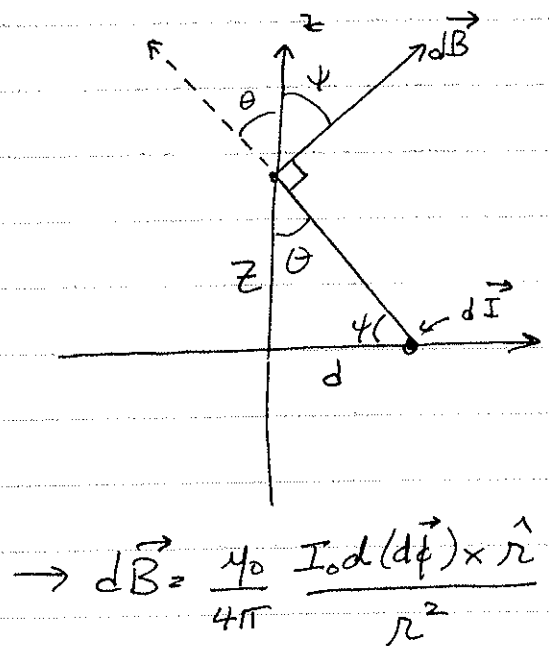
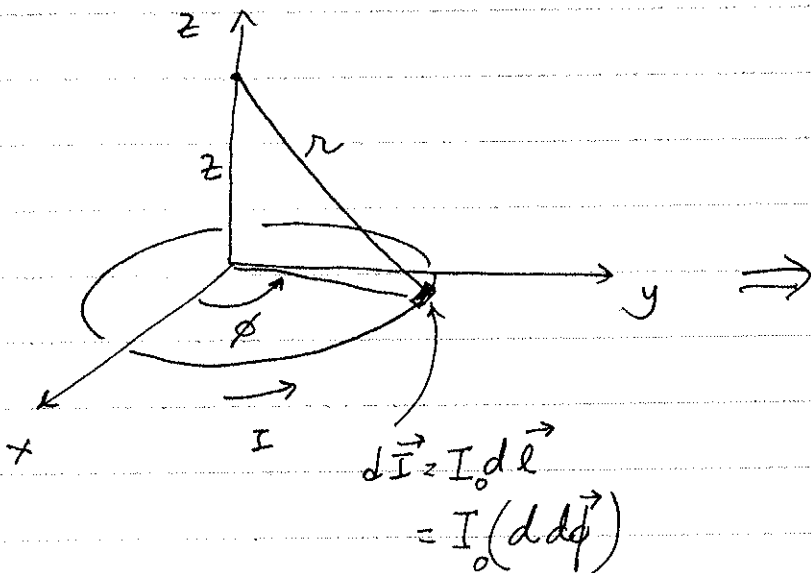
$$= -\frac{\mu_0 \sigma \Omega a}{2} \left[ \cos \theta - \frac{1}{3} \cos^3 \theta \right]_0^\pi$$

$$\vec{B} = \frac{2\mu_0 \sigma \Omega a}{2} \hat{z} = \frac{\mu_0 Q \Omega}{4\pi a} \hat{z}$$

# Helmholtz Coil



Find the  $\vec{B}$ -field on the z-axis at the midpoint of the above Helmholtz Coil.



$$\begin{aligned} d\vec{I} &= I_0 d\vec{l} \\ &= I_0 (d d\vec{\phi}) \end{aligned}$$

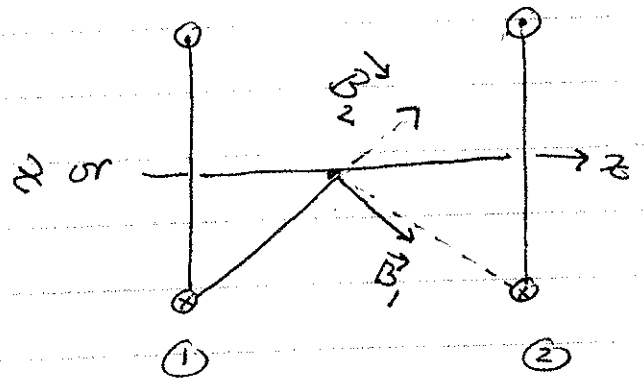
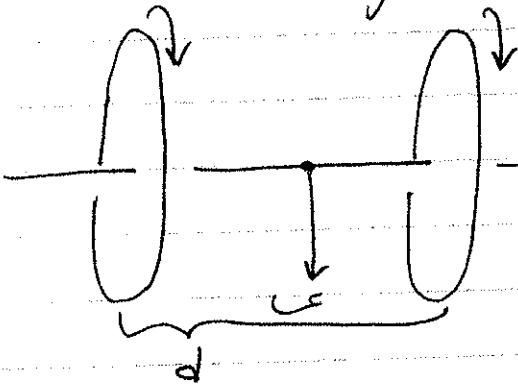
$$\rightarrow d\vec{B} = \frac{\mu_0}{4\pi} \frac{I_0 d (d\vec{\phi}) \times \hat{r}}{r^2}$$

(a) We note that, by symmetry, only the z-component of the  $d\vec{B}$  survives after integrating around the loop, and so,

$$\begin{aligned} dB_z &= \frac{\mu_0 I_0 d}{4\pi} \frac{d\phi}{r^2} \cos \psi = \frac{\mu_0 I_0 d}{4\pi} \frac{d\phi}{r^2} \left( \frac{d}{r} \right) \\ &= \frac{\mu_0 I_0 d^2}{4\pi (d^2 + z^2)^{3/2}} d\phi \end{aligned}$$

$$\rightarrow B = \frac{\mu_0 I_0}{4\pi} \left[ \frac{d^2}{(d^2 + z^2)^{3/2}} \right]$$

Return to 2 loop system



$$\vec{B}_{\text{tot}} = \left[ \frac{\mu_0 I}{2} \frac{d^2}{\left(d^2 + \left\{z + \frac{d}{2}\right\}^2\right)^{3/2}} + \frac{\mu_0 I}{2} \frac{d^2}{\left(d^2 + \left\{z - \frac{d}{2}\right\}^2\right)^{3/2}} \right] \hat{z}$$

at midpoint,  $z=0$

$$\vec{B}_{\text{tot}} = \frac{\mu_0 I}{d} \left[ \left(\frac{4}{5}\right)^{3/2} \hat{z} \right]$$

expand around origin,  $z=0$  or note that:

$$f(z) = f(0) + z f'(0) + \frac{z^2}{2!} f''(0) + \frac{z^3}{3!} f'''(0) + \dots$$

More interestingly,

$$\frac{\partial B}{\partial z} = \frac{\mu_0 I}{2} \left[ \frac{-3d^2 \left(z + \frac{d}{2}\right)}{\left(d^2 + \left[z + \frac{d}{2}\right]^2\right)^{5/2}} + \frac{-3d^2 \left(z - \frac{d}{2}\right)}{\left(d^2 + \left[z - \frac{d}{2}\right]^2\right)^{5/2}} \right]$$

at  $z=0$

$$\frac{\partial B}{\partial z} = 0 !$$

Further

$$\frac{\partial^2 B}{\partial z^2} = \frac{\mu_0 I}{2} (-3d^2) \left[ \frac{1}{(d^2 + [z + \frac{d}{2}]^2)^{5/2}} + \frac{1}{(d^2 + [z - \frac{d}{2}]^2)^{5/2}} - \frac{5(z + \frac{d}{2})^2}{(d^2 + [z + \frac{d}{2}]^2)^{7/2}} - \frac{5(z - \frac{d}{2})^2}{(d^2 + [z - \frac{d}{2}]^2)^{7/2}} \right]$$

at  $z=0$

$$\frac{\partial^2 B}{\partial z^2} = -\frac{3}{2} \mu_0 I d^2 \left[ \frac{2}{(5d^2/4)^{5/2}} - \frac{(5/2)d^2}{(5d^2/4)^{7/2}} \right]$$

$$= -3 \frac{\mu_0 I d^2}{(5d^2/4)^{5/2}} \left[ 1 - \frac{(5/4)d^2}{(5/4)d^2} \right]$$

$$= 0!$$

So, the field in a Helmholtz coil at  $z \approx 0$  is

$$B(z=0) = \frac{\mu_0 I}{d} \left( \frac{4}{5} \right)^{3/2}$$

and

$$B(z) = \frac{\mu_0 I}{d} \left( \frac{4}{5} \right)^{3/2} + \mathcal{O}(z^4)$$

in the neighborhood of  $z=0$ !



## Vector Potential & Divergence of $\vec{B}$ & Curl of $\vec{B}$

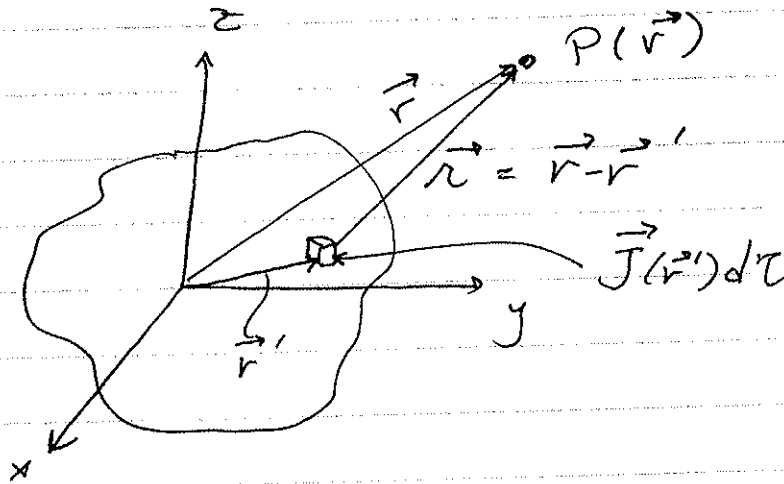
(ii) In ES,  $\vec{\nabla} \times \vec{E} = 0$ ,  $\vec{E} = -\vec{\nabla} V$ ,  $\oint \vec{E} \cdot d\vec{l} = 0$ ,  $\vec{E} \cdot d\vec{r} = -dV$ ,  
 $\int_A^B \vec{E} \cdot d\vec{r} = V(B) - V(A)$

(iii) What about MS?

### Biot-Savart law

$$\vec{B} = \frac{\mu_0}{4\pi} \int \vec{J}(\vec{r}') \times \frac{\hat{r}}{r^2} d\tau$$

where



Let's see what  $\vec{\nabla} \cdot \vec{B}$  and  $\vec{\nabla} \times \vec{B}$  are.

# Divergence

$$\vec{\nabla}_{\vec{r}} \cdot \vec{B} = \frac{\mu_0}{4\pi} \underbrace{\vec{\nabla}_{\vec{r}}}_{\substack{\text{derivative} \\ \text{w/ respect to} \\ \text{field point } \vec{r}}} \cdot \int \underbrace{\vec{J}(\vec{r}')}_{\substack{\text{independent of } \vec{r} \\ \text{the integration position vector}}} \times \frac{\hat{r}}{r^2} d\tau$$

$$= \frac{\mu_0}{4\pi} \int \vec{\nabla}_{\vec{r}} \cdot \left[ \vec{J}(\vec{r}') \times \frac{\hat{r}}{r^2} \right] d\tau$$

$$\text{ID\#6} = \frac{\mu_0}{4\pi} \int \left[ \frac{\hat{r}}{r^2} \cdot (\vec{\nabla}_{\vec{r}} \times \vec{J}(\vec{r}')) - \vec{J}(\vec{r}') \cdot (\vec{\nabla}_{\vec{r}} \times \frac{\hat{r}}{r^2}) \right] d\tau$$

$\vec{J}$  depends only on  $\vec{r}'$

Q: what is  $\vec{\nabla}_{\vec{r}} \times \left( \frac{\hat{r}}{r^2} \right)$  ?

$$\vec{\nabla}_{\vec{r}} \times \left( \frac{\hat{r}}{r^2} \right) = \left( \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right) \times \left( \frac{x-x'}{r^3}, \frac{y-y'}{r^3}, \frac{z-z'}{r^3} \right)$$

$$= \left[ -\frac{(z-z')}{r^5} (3[y-y']) + \frac{(y-y')}{r^5} 3(z-z'), \dots, \dots \right]$$

$$= (0, 0, 0)$$

take limit as  $x \rightarrow x'$   
 $y \rightarrow y'$   
 $z \rightarrow z'$

$$\Rightarrow \boxed{\vec{\nabla} \cdot \vec{B} = 0}$$

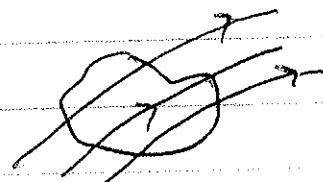
$\Rightarrow$  no sources or sinks of  $\vec{B}$ -field  $\Rightarrow$  no magnetic charges, no monopoles

"Gauss's Theorem"

$$\int (\vec{\nabla} \cdot \vec{B}) d\tau = 0$$

$$\boxed{\oint \vec{B} \cdot d\vec{S} = 0}$$

closed surface  $\Rightarrow$



# Curl

$$\vec{\nabla}_{\vec{r}} \times \vec{B} = \frac{\mu_0}{4\pi} \vec{\nabla}_{\vec{r}} \times \int \left[ \vec{J}(\vec{r}') \times \frac{\hat{r}}{r^2} d\tau \right] ?$$

ID #8

$$= \frac{\mu_0}{4\pi} \int \left[ \left( \frac{\hat{r}}{r^2} \cdot \vec{\nabla}_{\vec{r}} \right) \vec{J}(\vec{r}') - \left( \vec{J}(\vec{r}') \cdot \vec{\nabla}_{\vec{r}} \right) \frac{\hat{r}}{r^2} + \vec{J}(\vec{r}') \left( \vec{\nabla}_{\vec{r}} \cdot \frac{\hat{r}}{r^2} \right) - \frac{\hat{r}}{r^2} \left( \vec{\nabla}_{\vec{r}} \cdot \vec{J}(\vec{r}') \right) \right] d\tau$$

*depends only on  $\vec{r}'$*   
*if steady current*

$4\pi \delta^3(\vec{r})$

Q: what is

$$-\frac{\mu_0}{4\pi} \int \left( \vec{J}(\vec{r}') \cdot \vec{\nabla}_{\vec{r}} \right) \frac{\hat{r}}{r^2} d\tau ?$$

$$\vec{\nabla} \cdot \vec{J} + \frac{\partial \rho}{\partial t} = 0$$

note:  $\left[ \vec{J}(\vec{r}') \cdot \vec{\nabla}_{\vec{r}} \right] \frac{\hat{r}}{r^2} = - \left[ \vec{J}(\vec{r}') \cdot \vec{\nabla}_{\vec{r}'} \right] \frac{\hat{r}}{r^2}$ , because  $\vec{r} = \vec{r} - \vec{r}'$

and so, we have

$$\frac{\mu_0}{4\pi} \int \left[ \vec{J}(\vec{r}') \cdot \vec{\nabla}_{\vec{r}'} \right] \frac{\hat{r}}{r^2} d\tau = ? \leftarrow \left( \vec{J}(\vec{r}') \cdot \vec{\nabla}_{\vec{r}'} \right) \left( \frac{x-x'}{r^3} \right)$$

x-comp: Use vector ID,  $\vec{\nabla} \cdot (f\vec{A}) = f(\vec{\nabla} \cdot \vec{A}) + (\vec{A} \cdot \vec{\nabla})f$

$$\left( \vec{J} \cdot \vec{\nabla}_{\vec{r}'} \right) \left( \frac{x-x'}{r^3} \right) = \vec{\nabla}_{\vec{r}'} \cdot \left[ \frac{x-x'}{r^3} \vec{J} \right] - \left( \frac{x-x'}{r^3} \right) \underbrace{\vec{\nabla}_{\vec{r}'} \cdot \vec{J}(\vec{r}')}$$

recall:

Continuity Equation

$$\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot \vec{J} = 0$$

$\rightarrow \vec{\nabla} \cdot \vec{J} = 0$  in steady state

$$(\vec{J} \cdot \vec{\nabla}_{r'}) \left( \frac{x-x'}{r^3} \right) = \vec{\nabla}_{r'} \cdot \left[ \frac{(x-x')}{r^3} \vec{J} \right]$$

and the x-comp integral is

$$-\frac{\mu_0}{4\pi} \int \vec{\nabla}_{r'} \cdot \left[ \frac{x-x'}{r^3} \vec{J} \right] d\tau$$

$$= -\frac{\mu_0}{4\pi} \oint \left( \frac{x-x'}{r^3} \right) \vec{J} \cdot d\vec{S}$$

if Volume encloses all  $\vec{J} \Rightarrow \vec{J} \cdot d\vec{S} = 0$  and

$$\Rightarrow \phi = 0$$

$$\Rightarrow -\frac{\mu_0}{4\pi} \int \left[ \vec{J}(\vec{r}') \cdot \vec{\nabla}_r \right] \frac{r}{r^2} d\tau = 0$$

and

$$\vec{\nabla} \times \vec{B} = \frac{\mu_0}{4\pi} \int \vec{J}(\vec{r}') 4\pi f^3(r\vec{r}) d\tau$$

note:  $\vec{r} = 0 \Rightarrow \vec{J}$  is evaluated at  $\vec{r}' = \vec{r}$

$$\boxed{\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}(\vec{r})}, \vec{J}(\vec{r}) \text{ doesn't extend to } \infty$$

and  $\frac{\partial}{\partial t} = 0$

Ampere's Law

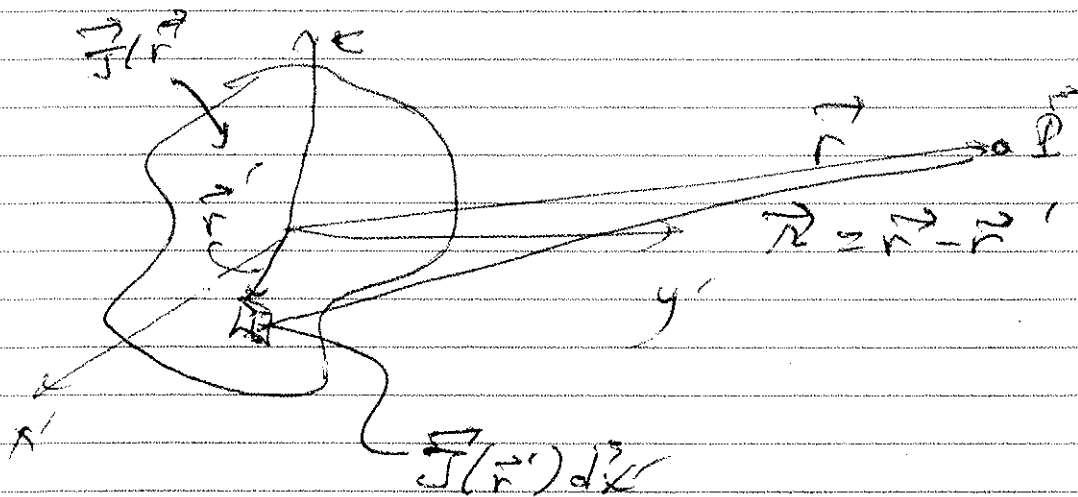
Stokes's thm  $\Rightarrow \oint (\vec{\nabla} \times \vec{B}) \cdot d\vec{S} = \mu_0 \int \vec{J}(\vec{r}) \cdot d\vec{S}$

Stokes's theorem  $\Rightarrow \oint \vec{B} \cdot d\vec{\ell} = \mu_0 \int \vec{J}(\vec{r}) \cdot d\vec{S}$

# Biot-Savart law

$$\vec{B} = \frac{\mu_0}{4\pi} \int \frac{\vec{J} d^3x' \times \hat{r}}{r^2}$$

is useful in that it gives the field from an arbitrary current distribution. However, as in electrostatics it is useful to have differential forms to get  $\vec{B}$ .



Recall:  $\frac{\hat{r}}{r^2} = -\vec{\nabla}_r \left( \frac{1}{r} \right)$

reverse order and pull out  $\vec{\nabla}_r \times$

$$\Rightarrow \vec{B} = \frac{\mu_0}{4\pi} \int (\vec{J}(r') d^3x') \times \left( -\vec{\nabla}_r \frac{1}{r} \right)$$

$$\vec{B} = \frac{\mu_0}{4\pi} \vec{\nabla}_r \times \int \frac{\vec{J}(r') d^3x'}{r}$$

independent of  $r'$   
 must stay under  $\int$  sign

$$(1) \quad \vec{\nabla} \cdot \vec{B}$$

$$\vec{\nabla} \cdot \vec{B} = \frac{\mu_0}{4\pi} \vec{\nabla}_r \cdot \left[ \vec{\nabla}_r \times \int \frac{\vec{J}(\vec{r}') d^3x'}{r} \right]$$

→ 0

$$\boxed{\vec{\nabla}_r \cdot \vec{B} = 0}$$

$$(2) \quad \vec{\nabla} \times \vec{B}$$

$$\vec{\nabla} \times \vec{B} = \frac{\mu_0}{4\pi} \vec{\nabla}_r \times \left[ \vec{\nabla}_r \times \int \frac{\vec{J}(\vec{r}') d^3x'}{r} \right]$$

$$\text{ID \# 11} \quad \vec{\nabla} \times (\vec{\nabla} \times \vec{A}) = \vec{\nabla} (\vec{\nabla} \cdot \vec{A}) - (\vec{\nabla} \cdot \vec{\nabla}) \vec{A}$$

$$\vec{\nabla} \times \vec{B} = \frac{\mu_0}{4\pi} \left\{ \underbrace{\vec{\nabla}_r \left( \vec{\nabla}_r \cdot \int \frac{\vec{J}(\vec{r}') d^3x'}{r} \right)}_a - \underbrace{(\vec{\nabla}_r \cdot \vec{\nabla}_r) \int \frac{\vec{J}(\vec{r}') d^3x'}{r}}_b \right\}$$

$$(a) \quad \vec{\nabla}_r \cdot \int \frac{\vec{J}(\vec{r}') d^3x'}{r} = \int \left( \vec{J}(\vec{r}') \cdot \vec{\nabla}_r \right) \frac{1}{r}$$

$$\vec{\nabla}_r \cdot \frac{1}{r} = -\vec{\nabla}_r \cdot \frac{1}{r}$$

$$\Rightarrow - \int \vec{J}(\vec{r}') d^3x' \cdot \vec{\nabla}_{\vec{r}} \left( \frac{1}{r} \right)$$

$$\textcircled{b} \vec{\nabla}_{\vec{r}} \cdot \vec{\nabla}_{\vec{r}} \int \frac{\vec{J}(\vec{r}') d^3x'}{r}$$

$$= \int \vec{J}(\vec{r}') d^3x' \vec{\nabla}_{\vec{r}} \cdot \vec{\nabla}_{\vec{r}} \left( \frac{1}{r} \right)$$

$$= \int \vec{J}(\vec{r}') d^3x' \underbrace{\vec{\nabla}_{\vec{r}} \cdot \left( \frac{\vec{r}}{r^2} \right)}_{4\pi \delta^3(\vec{r})}$$

and we have

$$\vec{\nabla} \times \vec{B} = - \frac{\mu_0}{4\pi} \vec{\nabla}_{\vec{r}} \int \vec{J}(\vec{r}') d^3x' \cdot \vec{\nabla}_{\vec{r}} \left( \frac{1}{r} \right) + \mu_0 \vec{J}(\vec{r})$$

note:  $\vec{\nabla}_{\vec{r}} \cdot \left[ \vec{J}(\vec{r}') \frac{1}{r} \right] = \frac{1}{r} \vec{\nabla}_{\vec{r}} \cdot \vec{J}(\vec{r}') + \vec{J}(\vec{r}') \cdot \vec{\nabla}_{\vec{r}} \frac{1}{r}$

$$\rightarrow \vec{\nabla} \times \vec{B} = \frac{\mu_0}{4\pi} \vec{\nabla}_{\vec{r}} \int \left\{ \frac{\vec{\nabla}_{\vec{r}} \cdot \vec{J}(\vec{r}') d^3x'}{r} - \vec{\nabla}_{\vec{r}} \cdot \left( \frac{\vec{J}(\vec{r}')}{r} \right) \right\}$$

$$\rightarrow 0, \frac{\partial \rho}{\partial t} = 0$$

$$\rightarrow \oint \frac{\vec{J}(\vec{r}')}{r} \cdot d\vec{S}$$

$$\rightarrow 0, \text{if } \vec{J} \text{ is not enclosed}$$

$$\Rightarrow \boxed{\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}}$$

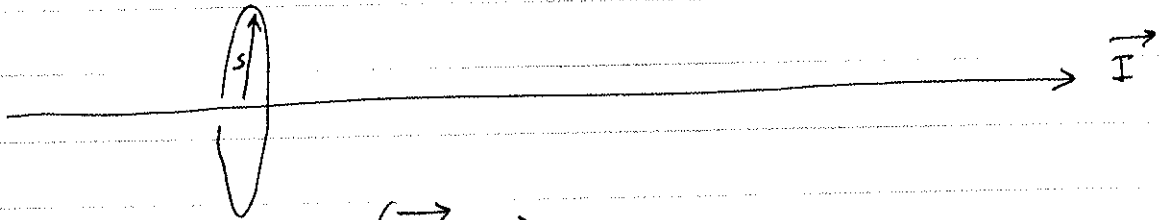
$$\Rightarrow \oint \vec{B} \cdot d\vec{l} = \mu_0 I$$

Ampere's law

## Examples

Ampere's law (plays role in Gauss's law in magnetostatics)

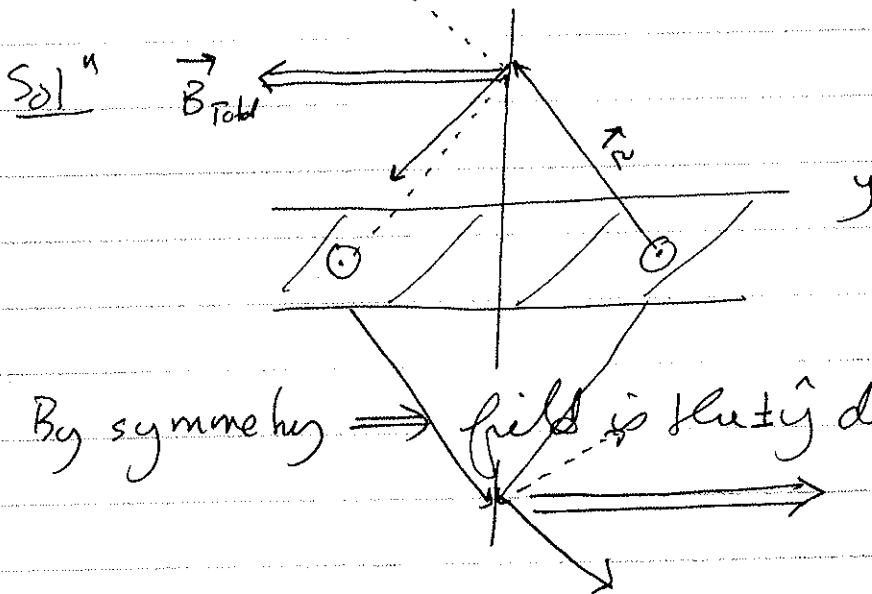
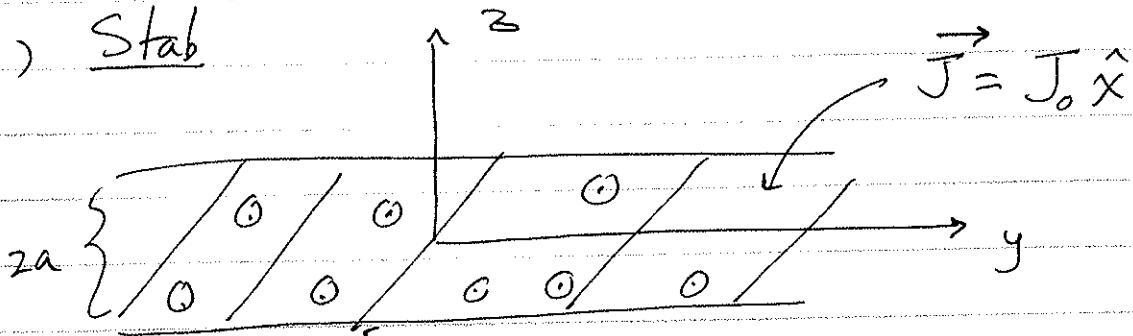
a) line current (wire)  $\Rightarrow B_\phi$ !



$$\oint \vec{B} \cdot d\vec{l} = \mu_0 \int \vec{J} \cdot d\vec{s} \Rightarrow B_\phi 2\pi s = \mu_0 I$$

$$\boxed{\vec{B}_\phi = \frac{\mu_0 I}{2\pi s} \hat{\phi}}$$

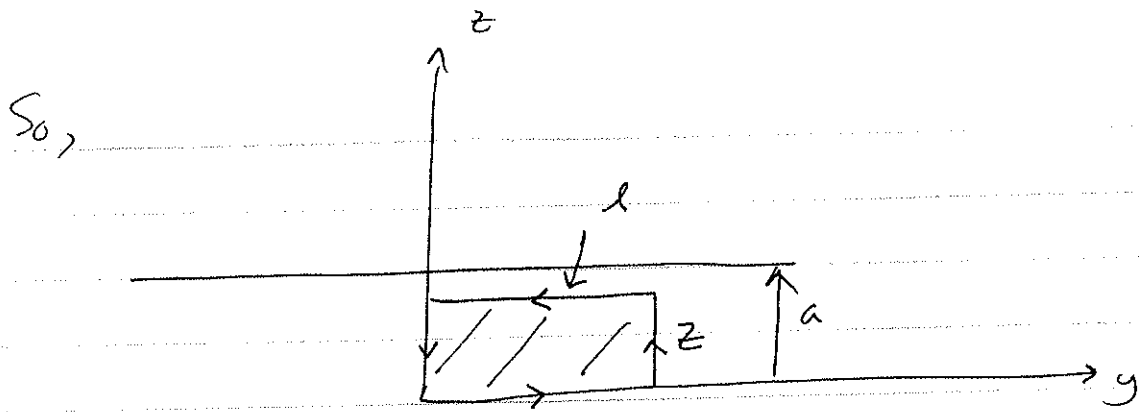
b) Stab



By symmetry  $\Rightarrow$  field is  $\pm \hat{y}$  direction

$\rightarrow B(z=a) = 0$  by symmetry





$$\oint \vec{B} \cdot d\vec{l} = \mu_0 \int \vec{J} \cdot d\vec{S} = \mu_0 J_0 l \begin{cases} z & , 0 < z < a \\ a & , a < z \end{cases}$$

$$-B_y(z)l - \cancel{B_y(z=0)l} = \mu_0 J_0 l \begin{cases} z & 0 < z < a \\ a & a < z \end{cases}$$

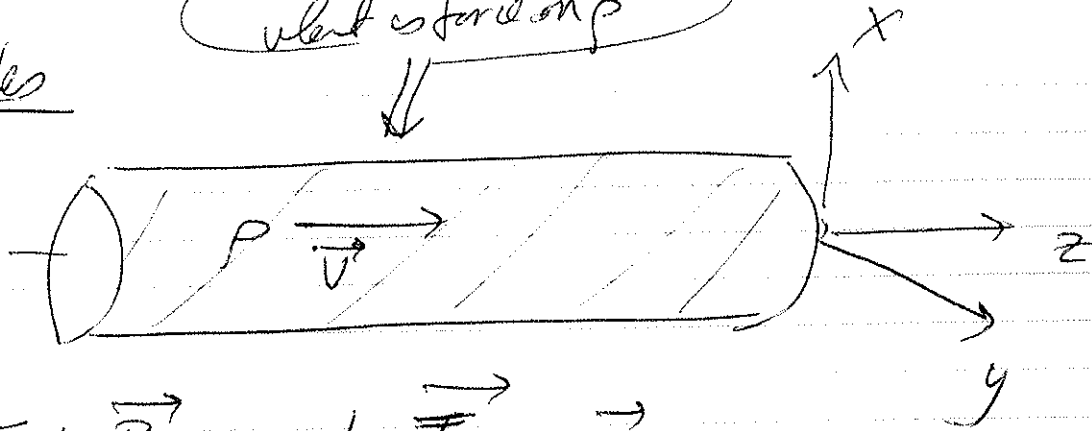
$$\rightarrow -B_y(z) = \begin{cases} \mu_0 J_0 z & 0 < z < a \\ \mu_0 J_0 a & a < z \end{cases}$$

by symmetry

$$+B_y(z) = \begin{cases} -\mu_0 J_0 z & 0 > z > -a \\ \mu_0 J_0 a & -a > z \end{cases}$$

Examples

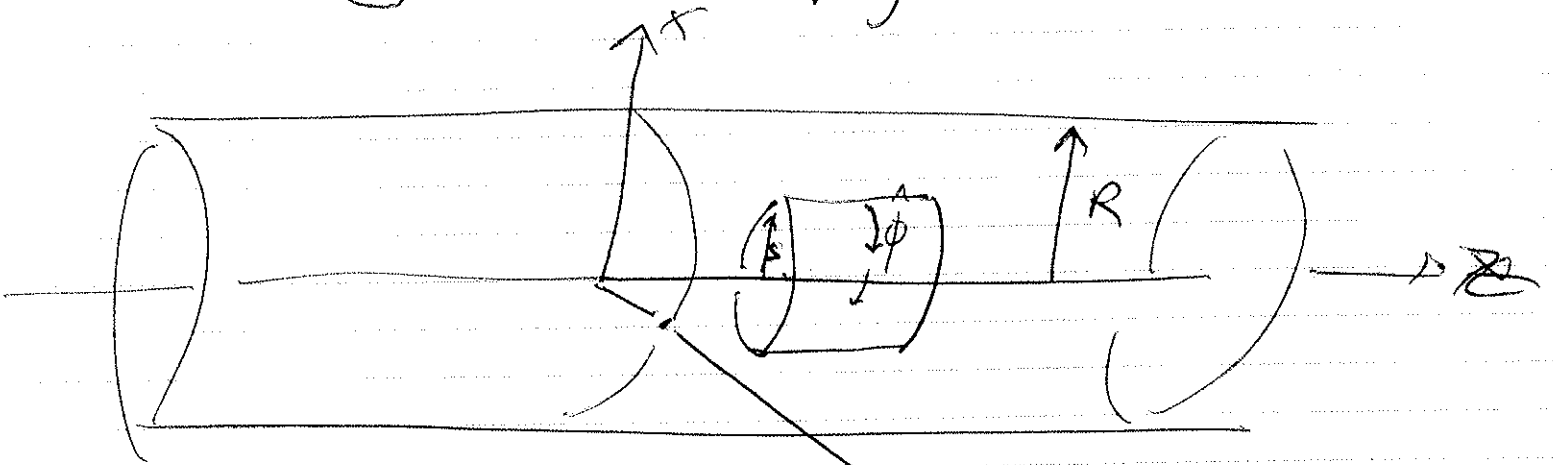
what is force on p?



a) Find  $\vec{B}$  due to  $\vec{J} = \rho \vec{v}$

(i) Use Ampere's law

$$\oint \vec{B} \cdot d\vec{l} = \mu_0 \int \vec{J} \cdot d\vec{S}$$



$$\Rightarrow a) \vec{B} \cdot 2\pi s \hat{\phi} = \rho \pi s^2 v \mu_0 \hat{z} \quad ; s < R$$

$$\text{and } B_{\phi} = \frac{\rho v \pi s^2}{2\pi s \mu_0} \Rightarrow \vec{B}_{\phi} = \mu_0 \frac{\rho v s}{2} \hat{\phi}$$

$$b) s > R \Rightarrow B_{\phi} = \frac{\rho v \pi R^2}{2\pi s \mu_0} \Rightarrow \vec{B}_{\phi} = \mu_0 \frac{\rho v R^2}{2s} \hat{\phi}$$

Force:

(a)  $d\vec{F} = \vec{J} d^3x \times \vec{B}$

$\Rightarrow d\vec{F} = -\rho v d^3x \left( \mu_0 \frac{\rho v}{2} \hat{s} \right) \hat{s}$

force inward (radially directed)

$\vec{F}_s = -\frac{\mu_0 \rho^2 v^2}{2} \int (s ds dz) \hat{s}$

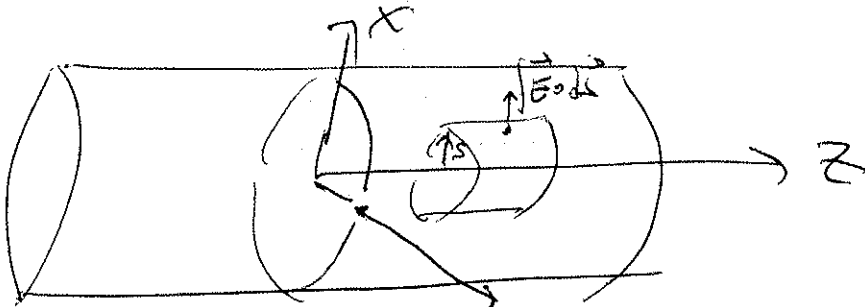
$= \frac{\mu_0 \rho^2 v^2}{2} \left[ 2\pi L \frac{s^3}{3} \right] \hat{s}$

$\vec{F}_s / L = -\frac{\mu_0 \rho^2 v^2 \pi s^3}{3} \hat{s}$

← force per unit length

Lorentz force

b)



$\vec{E}_s = \frac{\rho \pi s^2 L}{\epsilon_0 2\pi s L} \hat{s} = \frac{\rho s}{2\epsilon_0} \hat{s}$

Gauss's law

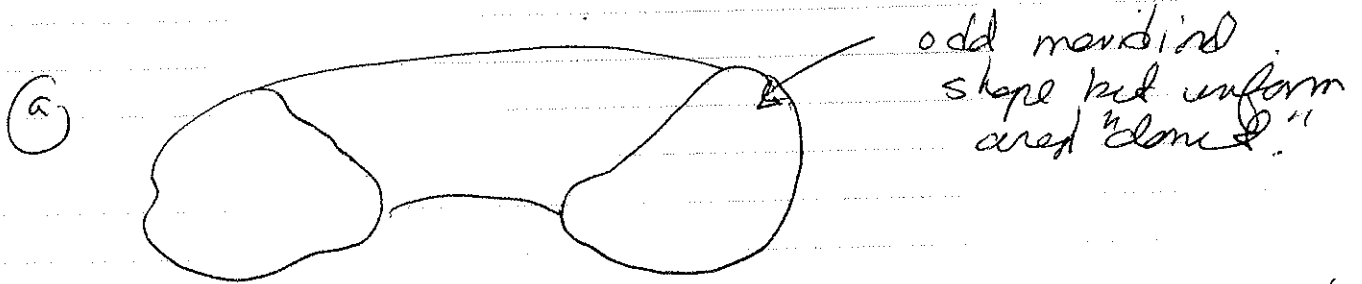
$\vec{F} = \int \frac{1}{2\epsilon_0} \rho s \rho (s ds dz)$

$= \frac{\pi \rho^2}{3} \left[ \frac{s^3}{3} L \right] \hat{s} \Rightarrow$

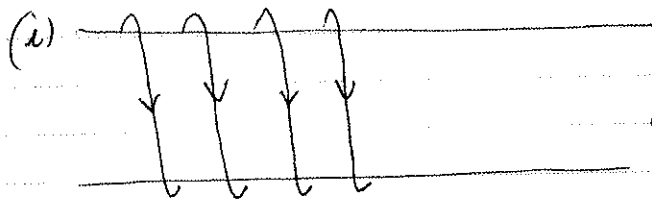
$\vec{F}_s / L = \frac{\pi \rho^2}{36\epsilon_0} s^3 \hat{s}$

compute

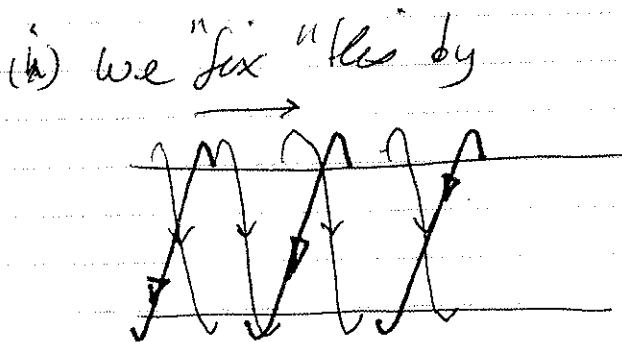
# "Toroidal (Donut)" loop



(b) wrap coils of wire tightly around perimeter (about the meridional slice) so that there is no current in  $\phi$  (around the loop). How do we accomplish this?



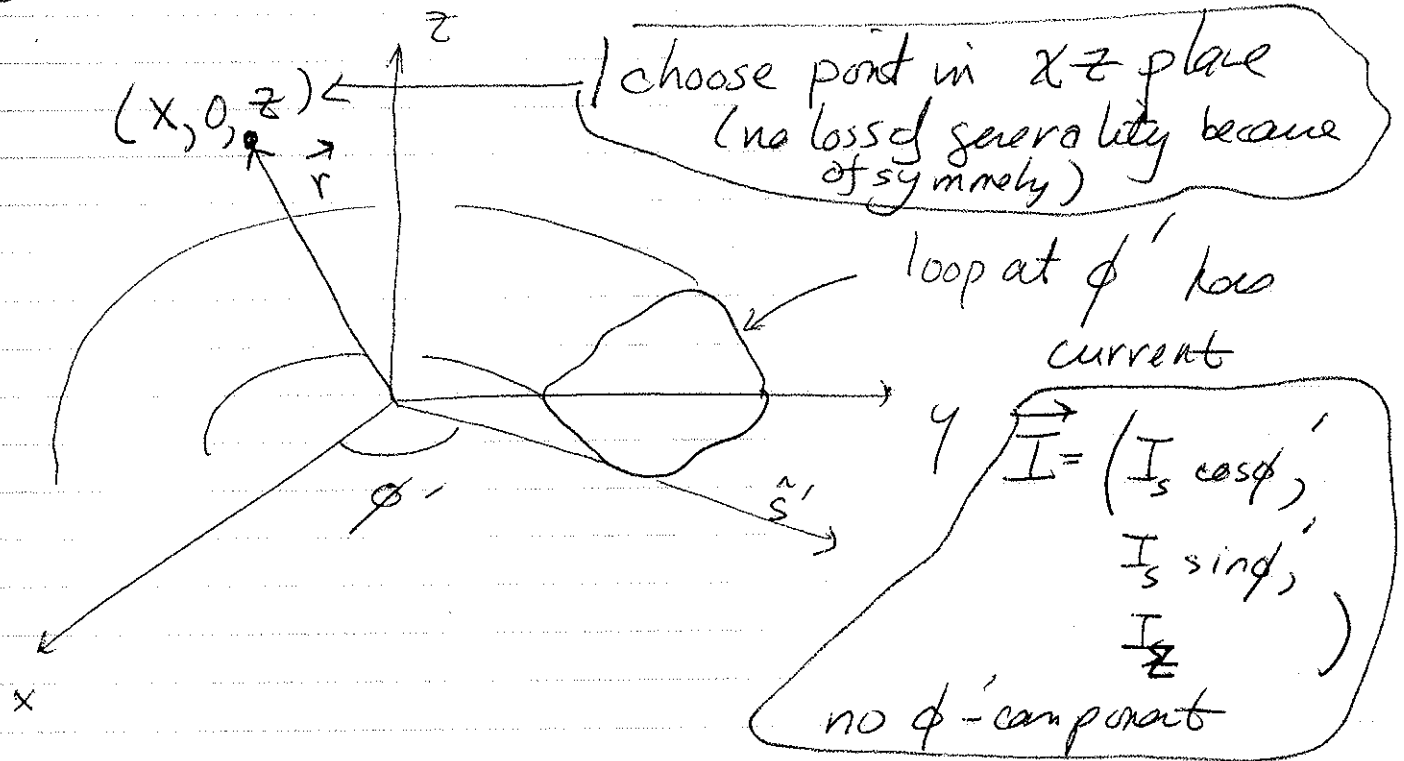
(i) However,  $I$  has  $\int + \rightarrow$   
that is, 2 components



(ii)  $I$  has  $\int + \leftarrow$   
again, 2 components

(i) + (ii)  $\Rightarrow \Leftrightarrow$  cancel, but  $\int$  add

Okay let's find  $\vec{B}$  due to the donut



Biot-Savart law

$$a) d\vec{B} = \frac{\mu_0}{4\pi} \frac{\vec{I} \times \hat{r}}{r^2} dl \quad \vec{r} = \vec{r} - \vec{r}' \quad y=0$$

$$= (x-x', y-y', z-z')$$

b) write down  $\vec{I} \times \vec{r}$

$$\vec{I} \times \vec{r} = (I_s \cos \phi', I_s \sin \phi', I_z) \times (x-x', -y', z-z')$$

$$= (I_s \sin \phi' [z-z'] + I_z y', I_z [x-x'] - I_s \cos \phi' [z-z'], I_s \cos \phi' [-y'] - I_s \sin \phi' [x-x'])$$

c) Integrate  $\vec{I} \times \vec{r}$  over loops

(d) First note that

$$(x', y', z') = (s' \cos \phi', s' \sin \phi', z')$$

$$\Rightarrow \vec{I} \times \vec{n} = \left( \sin \phi' \left[ I_3 (z-z') + I_2 s' \right], \right. \\ \left. \cos \phi' \left[ -s' I_2 - I_3 (z-z') \right] + x I_2, \right. \\ \left. - \sin \phi' \left[ I_3 x \right] + \cos \phi' \sin \phi' \left[ -s' I_3 + I_3 s' \right] \right)$$

$\rightarrow 0$

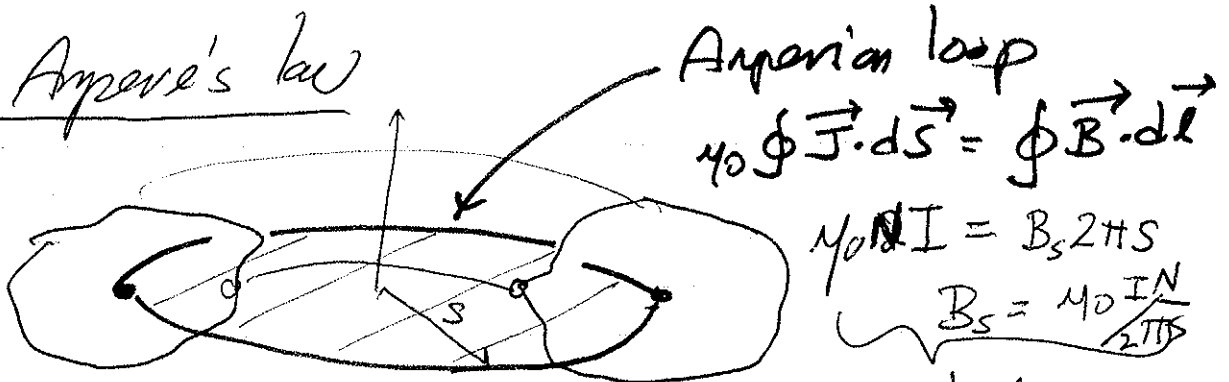
(e) { over a meridional slice,  $\phi'$  is fixed. So, when we do the int. eqn,  $s'$  also runs over the same interval as does  $z'$  and don't change int. eqn

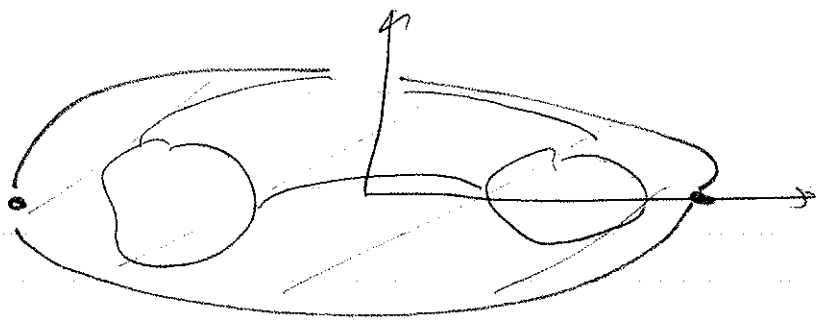
~~$\phi$  runs from  $0 \rightarrow 2\pi \Rightarrow \sin \phi', \cos \phi'$  also run~~  
 ~~$\rightarrow$  cancel over the int. eqn~~

~~(f)  $\Rightarrow \vec{I} \times \vec{n} = (0, x I_2, 0)$~~

$\rightarrow$  field pts in  $\phi$  direction

(g) Use Ampere's law





$$\mu_0 \oint \vec{J} \cdot d\vec{S} = 0$$

$$= B_s 2\pi s$$

$$\Rightarrow B_s = 0$$

and the field is

$$\vec{B} = \frac{1}{s} \left\{ \begin{array}{l} \frac{\mu_0 N I}{2\pi s} \quad , \quad s \text{ inside} \\ 0 \quad , \quad s \text{ outside} \end{array} \right.$$

① Tokomaks work on this idea

- a) instabilities
  - b) curvature drift
  - c) gradient drift
  - d)  $\vdots$
- } bad

bad  $\Rightarrow$  Tokomaks use helical fields:

- (i) Current flow  $\rho V \phi \Rightarrow$  poloidal field
- (ii) Solenoidal field  $\Rightarrow$  toroidal field

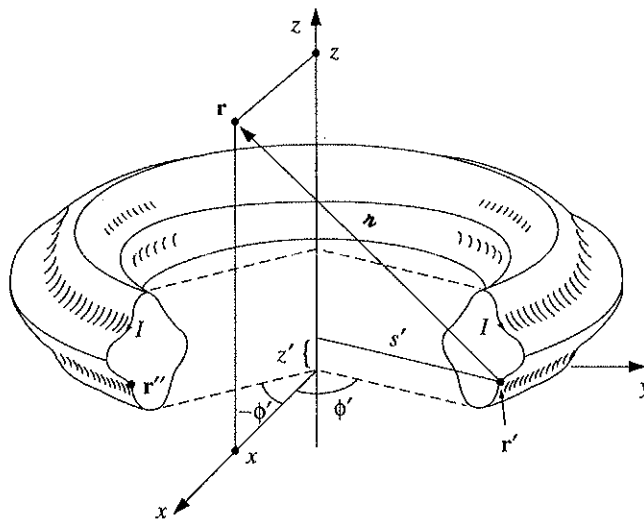


Figure 5.39

Accordingly,

$$\begin{aligned} \mathbf{I} \times \mathbf{z} &= \begin{bmatrix} \hat{x} & \hat{y} & \hat{z} \\ I_s \cos \phi' & I_s \sin \phi' & I_z \\ (x - s' \cos \phi') & (-s' \sin \phi') & (z - z') \end{bmatrix} \\ &= [\sin \phi' (I_s (z - z') + s' I_z)] \hat{x} \\ &\quad + [I_z (x - s' \cos \phi') - I_s \cos \phi' (z - z')] \hat{y} + [-I_s x \sin \phi'] \hat{z}. \end{aligned}$$

But there is a symmetrically situated current element at  $\mathbf{r}''$ , with the same  $s'$ , the same  $z$ , the same  $dl'$ , the same  $I_s$ , and the same  $I_z$ , but *negative*  $\phi'$  (Fig. 5.39). Because  $\sin \phi'$  changes sign, the  $\hat{x}$  and  $\hat{z}$  contributions from  $\mathbf{r}'$  and  $\mathbf{r}''$  cancel, leaving only a  $\hat{y}$  term. Thus the field at  $\mathbf{r}$  is in the  $\hat{y}$  direction, and in general the field points in the  $\hat{\phi}$  direction. *qed*

Now that we know the field is circumferential, determining its magnitude is ridiculously easy. Just apply Ampère's law to a circle of radius  $s$  about the axis of the toroid:

$$B 2\pi s = \mu_0 I_{\text{enc}},$$

and hence

$$\mathbf{B}(\mathbf{r}) = \begin{cases} \frac{\mu_0 N I}{2\pi s} \hat{\phi}, & \text{for points inside the coil,} \\ 0, & \text{for points outside the coil,} \end{cases} \quad (5.58)$$

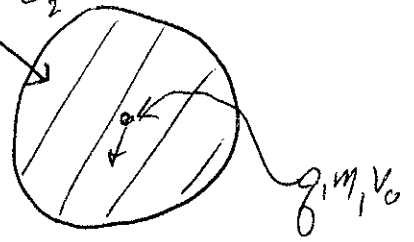
where  $N$  is the total number of turns.



Prob 5.41  $\equiv$  problem  $\longrightarrow \vec{B}(s) = B_r(s) \hat{z}$

$$a) \begin{cases} \ddot{x} = \dot{y} \left( \frac{qB(s)}{m} \right) \\ \ddot{y} = -\dot{x} \left( \frac{qB(s)}{m} \right) \\ \ddot{z} = 0 \end{cases}$$

from earlier lecture



if  $m$  escapes radially, show that

$$\oint \vec{B}(s) \cdot d\vec{A} = 0$$

b) Torque,  $\vec{N} = \vec{r} \times \vec{F}$

$\vec{L} = \vec{r} \times \vec{p}$

$$= (0, 0, -x\dot{x} \left[ \frac{qB(s)}{m} \right] - y\dot{y} \left[ \frac{qB(s)}{m} \right])$$

$$\frac{d\vec{L}}{dt} = (0, 0, - \left[ \frac{qB(s)}{m} \right] \frac{1}{2} \frac{d}{dt} (x^2 + y^2))$$

$$\int \frac{dL_z}{dt} dt = - \frac{q}{2m} \int B(s) \frac{d}{dt} (x^2 + y^2) dt$$

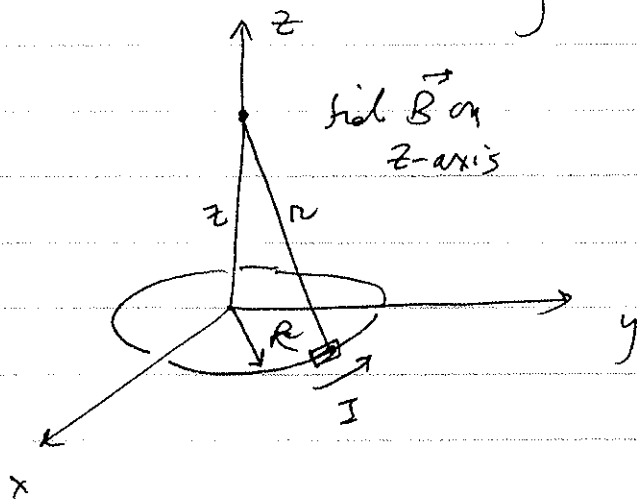
$$L_z \Big|_{t=0}^{t_{esc}} = - \frac{q}{2m} \int_{s=0}^R B(s) s ds$$

$$L_z(R) - L_z(0) = - \frac{q}{4\pi m} \int \vec{B}(s) \cdot d\vec{A}$$

$\uparrow$   
 $m$  moves radially  
 $\Rightarrow \vec{L}$  about origin is 0

## Approximation Scheme

a) look at the field of a wire loop



$$dB_z = \frac{\mu_0}{4\pi} \frac{IR d\phi R}{r^3}$$

$$\boxed{B_z = \frac{\mu_0 IR^2}{2(R^2+z^2)^{3/2}} \hat{z}}$$

b) Can we infer something about the field near the z-axis?

Yes, let's use  $\vec{\nabla} \cdot \vec{B}$  &  $\vec{\nabla} \times \vec{B}$

(i)  $\vec{\nabla} \cdot \vec{B} = 0$  0, by symmetry

$$\vec{\nabla} \cdot \vec{B} = \frac{1}{s} \frac{\partial}{\partial s} (s B_s) + \frac{1}{s} \frac{\partial}{\partial \phi} (B_\phi) + \frac{\partial}{\partial z} B_z = 0$$

we know  $\vec{B}$  on the z-axis ( $s=0$ ). Use this to find  $B_s$  &  $B_z$  off-axis

$$\vec{\nabla} \cdot \vec{B} = \frac{1}{s} \frac{\partial}{\partial s} (s B_s) + \frac{\partial}{\partial z} (B_z) = 0$$

$$\begin{aligned} \rightarrow \frac{1}{s} \frac{\partial}{\partial s} (s B_s) &= - \frac{\partial B_z}{\partial z} = - \frac{\mu_0 IR^2}{2} \left( - \frac{3z}{(R^2+z^2)^{5/2}} \right) \\ &= - \frac{3\mu_0 IR^2}{2} \left( \frac{-z}{(R^2+z^2)^{5/2}} \right) \end{aligned}$$

$$\rightarrow s B_s \Big|_0^s \approx \frac{3\mu_0 I R^2}{2} \left[ \frac{z}{(R^2+z^2)^{3/2}} \right] \frac{s^2}{2} \Big|_0^s$$

$$\rightarrow \boxed{\vec{B}_s(s, z) \approx \frac{3\mu_0 I R^2}{4} \left[ \frac{s z}{(R^2+z^2)^{3/2}} \right] \hat{s}}$$

(ii) Use  $\vec{\nabla} \times \vec{B} = \mu_0 \vec{J} = 0$  to find  $\vec{B}_z(s, z)$

$$\vec{\nabla} \times \vec{B} = 0 + \hat{\phi} \left[ \frac{\partial}{\partial z} B_s - \frac{\partial}{\partial s} B_z \right] + 0$$

$$\rightarrow \frac{\partial B_s}{\partial z} = \frac{\partial B_z}{\partial s}$$

from above  $= \frac{3\mu_0 I R^2}{4} \left[ s \left( \frac{R^2 - 4z^2}{(R^2+z^2)^{3/2}} \right) \right]$

integrate

$$B_z \Big|_0^s = \frac{3\mu_0 I R^2}{8} s^2 \left[ \frac{R^2 - 4z^2}{(R^2+z^2)^{3/2}} \right] \Big|_0^s$$

$$B_z(s, z) = B_z(0, z) + \frac{3\mu_0 I R^2}{8} \left( \frac{R^2 - 4z^2}{(R^2+z^2)^{3/2}} \right) s^2$$

↑  
phy in z on axis field

$$\boxed{\vec{B}_z = \frac{\mu_0 I R^2}{2 (R^2+z^2)^{3/2}} \left[ 1 + \frac{3}{4} \frac{(R^2 - 4z^2)}{(R^2+z^2)^2} s^2 \right] \hat{z}}$$

## Steady State Maxwell Equations

$$\left[ \begin{array}{ll} \vec{\nabla} \cdot \vec{E} = \rho / \epsilon_0 & \vec{\nabla} \cdot \vec{B} = 0 \\ \vec{\nabla} \times \vec{E} = 0 & \vec{\nabla} \times \vec{B} = \mu_0 \vec{J} \end{array} \right.$$

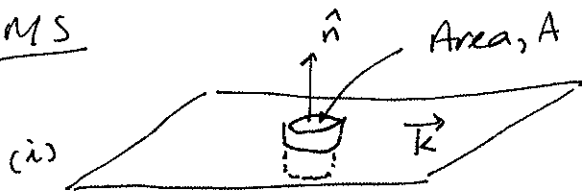
$$\left[ \begin{array}{ll} \oint \vec{E} \cdot d\vec{S} = \frac{1}{\epsilon_0} \int \rho d\tau & \oint \vec{B} \cdot d\vec{S} = 0 \\ \oint \vec{E} \cdot d\vec{l} = 0 & \oint \vec{B} \cdot d\vec{l} = \mu_0 \int \vec{J} \cdot d\vec{S} \end{array} \right.$$

Comment,  $\vec{\nabla} \cdot$ ,  $\vec{\nabla} \times$  are sufficient to describe an arbitrary vector field  
(Appendix B: Helmholtz Theorem)  
See given BCs.

## Boundary Conditions

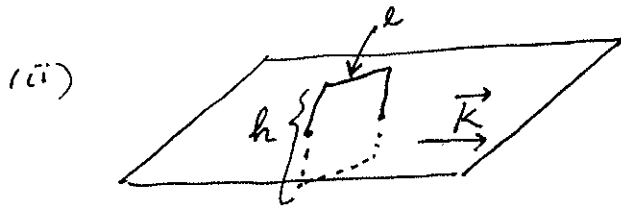
ES  
 (i)  $\Delta E_n = \sigma / \epsilon_0$  ,  $\Delta E_T = 0$

MS



$$\vec{\nabla} \cdot \vec{B} = 0$$

$$B_n^+ A - B_n^- A = \int \vec{K} \cdot d\vec{S} = 0 \Rightarrow \Delta B_n = 0$$



$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$$

$$\oint \vec{B} \cdot d\vec{l} = \mu_0 \int \vec{J} \cdot d\vec{S} \leftarrow \begin{array}{l} \text{the normal to } d\vec{S} \\ \text{is } \theta \end{array}$$

Top  $\Rightarrow$   $\Rightarrow \vec{J} \cdot d\vec{S} = J dS \cos \theta = Kl \cos \theta$

$$+ B_T^+ l - B_T^- l = \mu_0 Kl \cos \theta$$

$\nwarrow$  In the plane of the sheets,  $\angle(\vec{J}, d\vec{S}) = \theta$

$$\Delta B_T = \begin{cases} 0 & \vec{K} \parallel \vec{B} \\ \mu_0 K & \vec{K} \perp \vec{B} \end{cases}$$

## Vector Potential

Exploit  $\vec{\nabla} \cdot \vec{B} = 0$

Define a fun. which is  $\perp$  to  $\vec{B}$ ,

$$\vec{B} = \vec{\nabla} \times \vec{A} \quad \leftarrow \vec{A} \text{ is the vector potential}$$

$$\rightarrow \vec{\nabla} \cdot \vec{B} = \vec{\nabla} \cdot (\vec{\nabla} \times \vec{A}) \stackrel{\text{by def.}}{=} 0$$

a) Is this it? No, similar to the scalar potential  $V$ , where

$$\vec{E} = -\vec{\nabla} V$$

we could add any <sup>constant</sup> scalar to  $V$  and leave  $\vec{E}$  untouched,

$$\vec{E} = -\vec{\nabla}(V + f_0) = -\vec{\nabla} V - \vec{\nabla} f_0 \quad \leftarrow \vec{\nabla} f_0 = 0, f_0 = \text{const}$$

b) Add  $\vec{\nabla} f$  to  $\vec{A}$ . Note that

$$\vec{\nabla} \times (\vec{\nabla} f) = 0 \rightarrow \vec{B} \text{ is unchanged}$$

"Gauge freedom"  $\uparrow$

Q: How do we set the gauge?

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$$

$$\vec{\nabla} \times (\vec{\nabla} \times \vec{A}) = \mu_0 \vec{J}$$

Id #11)

$$\vec{\nabla}(\vec{\nabla} \cdot \vec{A}) - \underbrace{(\vec{\nabla} \cdot \vec{\nabla})}_{\nabla^2} \vec{A} = \mu_0 \vec{J}$$

$$\vec{\nabla}(\vec{\nabla} \cdot \vec{A}) - \nabla^2 \vec{A} = \mu_0 \vec{J}$$

define  $\vec{A} \ni \vec{\nabla} \cdot \vec{A} = 0$ . This can be accomplished because of  $\vec{\nabla} f \leftarrow$  gauge freedom.

okay  $\vec{\nabla} \cdot \vec{A} = 0$  is the "Coulomb gauge"

and we have

$$\Rightarrow \vec{\nabla} \cdot \vec{\nabla} \vec{A} = \nabla^2 \vec{A} = -\mu_0 \vec{J}, \text{ "Poisson's Eqn" for } \vec{A}$$

$$\Rightarrow \boxed{\vec{A} = \frac{\mu_0}{4\pi} \int \frac{\vec{J} d\tau}{r}}$$

as long as  $\vec{J}$  doesn't extend to infinity.

Connet

$$\int (\vec{\nabla} \cdot \vec{A}) d\tau = 0, \text{ from gauge condition}$$
$$\rightarrow \oint \vec{A} \cdot d\vec{S} = 0$$

\*

Addition to explain   on previous page

To see this,

$$\vec{B} = \vec{\nabla} \times \vec{A} = \vec{\nabla} \times \left[ \overbrace{A_0 + \vec{\nabla} f}^{\vec{A}} \right]$$

↑ some arbitrary function

$$\Rightarrow \vec{B} = \left\{ \vec{\nabla}(\vec{\nabla} \cdot \vec{A}_0) - \nabla^2 \vec{A}_0 \right\} + \left\{ \vec{\nabla}(\vec{\nabla} \cdot \vec{A}) - \nabla^2 \vec{A} \right\}$$

$$= \left\{ \vec{\nabla} \left[ \vec{\nabla} \cdot (\vec{A}_0 + \vec{\nabla} f) \right] - \nabla^2 [\vec{A}_0 + \vec{\nabla} f] \right\}$$

now,  $\vec{B} = \vec{\nabla} \times \vec{A}$  } contains the  $\vec{\nabla} \times$  of our def<sup>n</sup> of the vector field  $\vec{A}$ , however, we still need to specify the  $\vec{\nabla} \cdot$  behavior of  $\vec{A}$  to constrain  $\vec{A}$ .

we choose to set  $\vec{\nabla} \cdot \vec{A} = 0$ . This can be accomplished because of  $\vec{\nabla} f$

$$\Rightarrow \vec{\nabla} \cdot [\vec{A}_0 + \vec{\nabla} f] = 0 \Rightarrow \nabla^2 f = - \underbrace{\vec{\nabla} \cdot \vec{A}_0}_\rho$$

$$f = \frac{1}{4\pi} \int \frac{(\vec{\nabla} \cdot \vec{A}_0)}{r} d^3x'$$

$\Rightarrow \rho(\vec{\nabla} \cdot \vec{A}) \Rightarrow 0$  at  $\infty$ , we are okay



## Coulomb Gauge: Comments

Let's digress for a minute

$$a) \nabla \cdot \vec{E} = \rho/\epsilon_0$$

Gauss's law

$$b) \nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

Faraday's law (complete Maxwell Equation)

$$= -\frac{\partial}{\partial t} [\nabla \times \vec{A}]$$

$$\Rightarrow \nabla \times \left[ \vec{E} + \frac{\partial \vec{A}}{\partial t} \right] = 0$$

$\underbrace{\hspace{10em}}_{= -\nabla V}$

Now, plug in for  $\vec{E}$  in Gauss's law

$$\nabla \cdot \vec{E} = \nabla \cdot \left[ -\nabla V - \frac{\partial \vec{A}}{\partial t} \right] = \rho/\epsilon_0$$

$$-\nabla^2 V - \frac{\partial}{\partial t} [\nabla \cdot \vec{A}] = \rho/\epsilon_0$$

$$\Rightarrow \nabla^2 V = -\rho/\epsilon_0$$

in Coulomb gauge ( $\nabla \cdot \vec{A} = 0$ )

Unfortunately,

$$\vec{E} \neq -\nabla V(r, t),$$

$$\vec{E} = -\nabla V(r, t) - \frac{\partial \vec{A}}{\partial t}$$

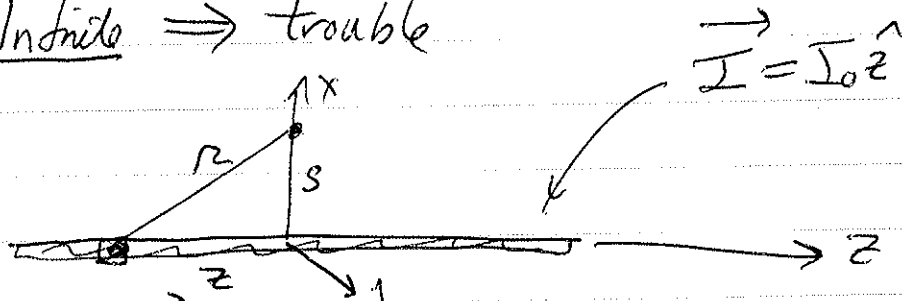
and it turns out  $\frac{\partial \vec{A}}{\partial t}$  is hard to find in general. In the time-dependent case, we use a more convenient gauge,

$$(\nabla \cdot \vec{A}) = -\mu_0 \epsilon_0 \frac{\partial V}{\partial t}$$

"Lorentz Gauge"

Find  $\vec{A}$  for an infinite line current

Infinite  $\Rightarrow$  trouble



①  $\vec{A}$  will be independent of  $z$ , by symmetry and so let's evaluate  $\vec{A}$  at  $z=0$ .

② To get around  $\infty$ , consider a wire of length  $2L$  and then let  $L \rightarrow \infty$

$$A_z = \frac{\mu_0}{4\pi} \int_{-L}^L \frac{I dz}{(s^2 + z^2)^{3/2}}$$

$$= \frac{\mu_0 I}{4\pi} \ln \left[ z + \sqrt{z^2 + s^2} \right]_{-L}^L$$

$$= \frac{\mu_0 I}{4\pi} \ln \left\{ \frac{L + \sqrt{L^2 + s^2}}{-L + \sqrt{s^2 + L^2}} \right\}$$

let  $L \rightarrow \infty$  ( $\Rightarrow L \gg s$ )

$$\approx \frac{\mu_0 I}{4\pi} \ln \left\{ \frac{L + L \left(1 + \frac{1}{2} \frac{s^2}{L^2}\right)}{-L + L \left(1 + \frac{1}{2} \frac{s^2}{L^2}\right)} \right\}$$

$$\begin{aligned}
A_z &\approx \frac{\mu_0 I}{4\pi} \left[ \ln \left( 2 + \frac{1}{2} \frac{s^2}{L^2} \right) - \ln \left( \frac{1}{2} \frac{s^2}{L^2} \right) \right] \\
&= \frac{\mu_0 I}{4\pi} \left[ \ln \left( \frac{1}{2L^2} [4L^2 + s^2] \right) - \ln \left( \frac{1}{2L^2} [s^2] \right) \right] \\
&= \frac{\mu_0 I}{4\pi} \left[ \ln (4L^2 + s^2) - \ln s^2 \right] \\
&= \frac{\mu_0 I}{4\pi} \left[ \ln 4L^2 + \ln \left( 1 + \frac{s^2}{4L^2} \right) - \ln s^2 \right]
\end{aligned}$$

$$A_z \approx \frac{\mu_0 I}{4\pi} \left[ \ln 4L^2 - \ln s^2 \right]$$

$\rightarrow \infty$   
 $\infty L \rightarrow \infty!$

However, it is a constant  $\Rightarrow \nabla \times \vec{A}_z$  is not affected by it and so can be dropped

$$\Rightarrow A_z \approx -\frac{\mu_0 I}{2\pi} \ln s$$

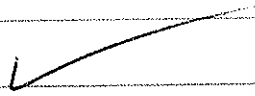
$$\infty L \rightarrow \infty$$

$$\textcircled{a} \vec{B} = \nabla \times \vec{A}$$

$$= \hat{s} \left( \frac{1}{s} \frac{\partial A_z}{\partial \phi} - \frac{\partial A_\phi}{\partial z} \right) + \hat{\phi} \left( \frac{\partial A_s}{\partial z} - \frac{\partial A_z}{\partial s} \right) + \hat{z} \frac{1}{s} \left( \frac{\partial}{\partial s} (s A_\phi) - \frac{\partial}{\partial \phi} A_s \right)$$

$$= \hat{s} [0 - 0] + \hat{\phi} \left[ 0 + \frac{\mu_0 I}{2\pi s} \right] + \hat{z} [0 - 0]$$

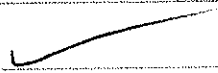
$$\boxed{\vec{B} = \frac{\mu_0 I}{2\pi s} \hat{\phi}}$$



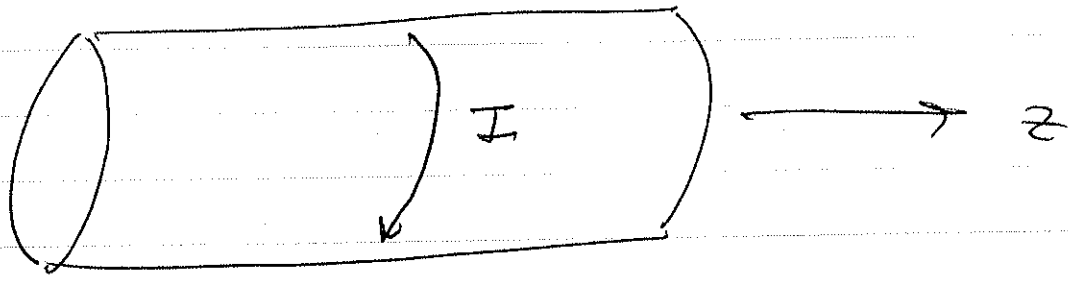
$$\textcircled{b} \nabla \cdot \vec{A} = \frac{1}{s} \frac{\partial}{\partial s} (s A_s) + \frac{1}{s} \frac{\partial}{\partial \phi} A_\phi + \frac{\partial}{\partial z} A_z$$

$$= 0 + 0 + 0$$

$$\boxed{\nabla \cdot \vec{A} = 0}$$

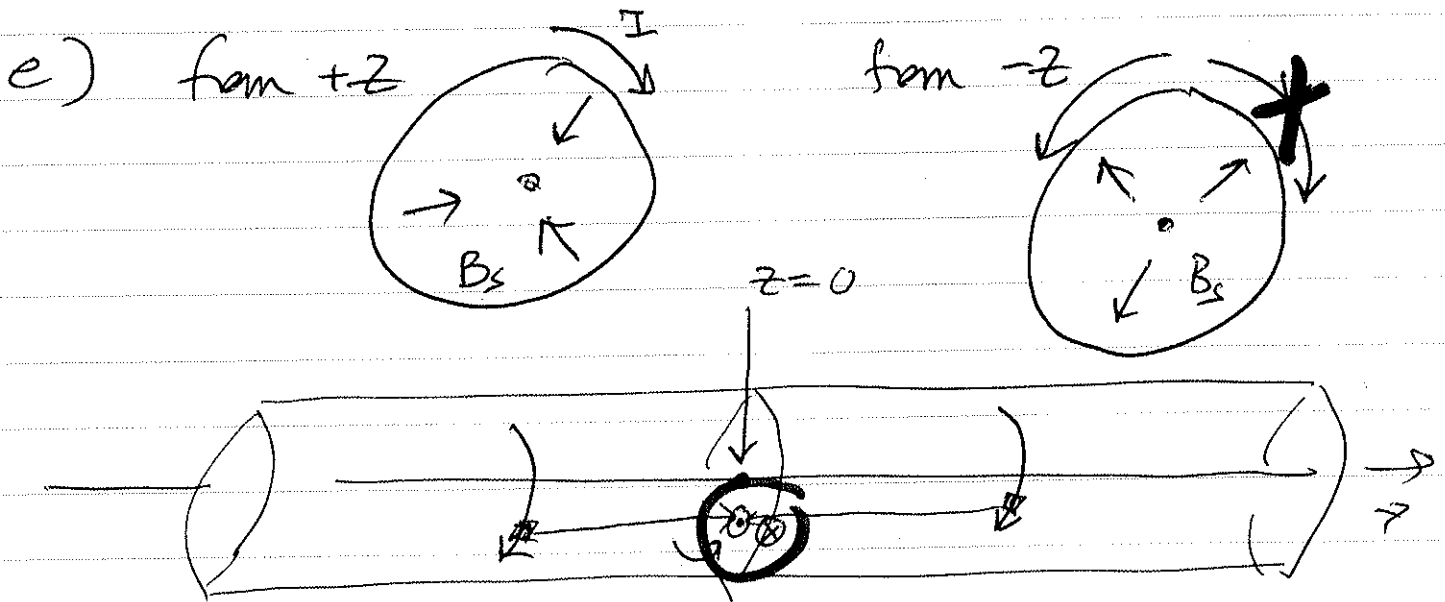


# Infinite Solenoid: find $\vec{A}$



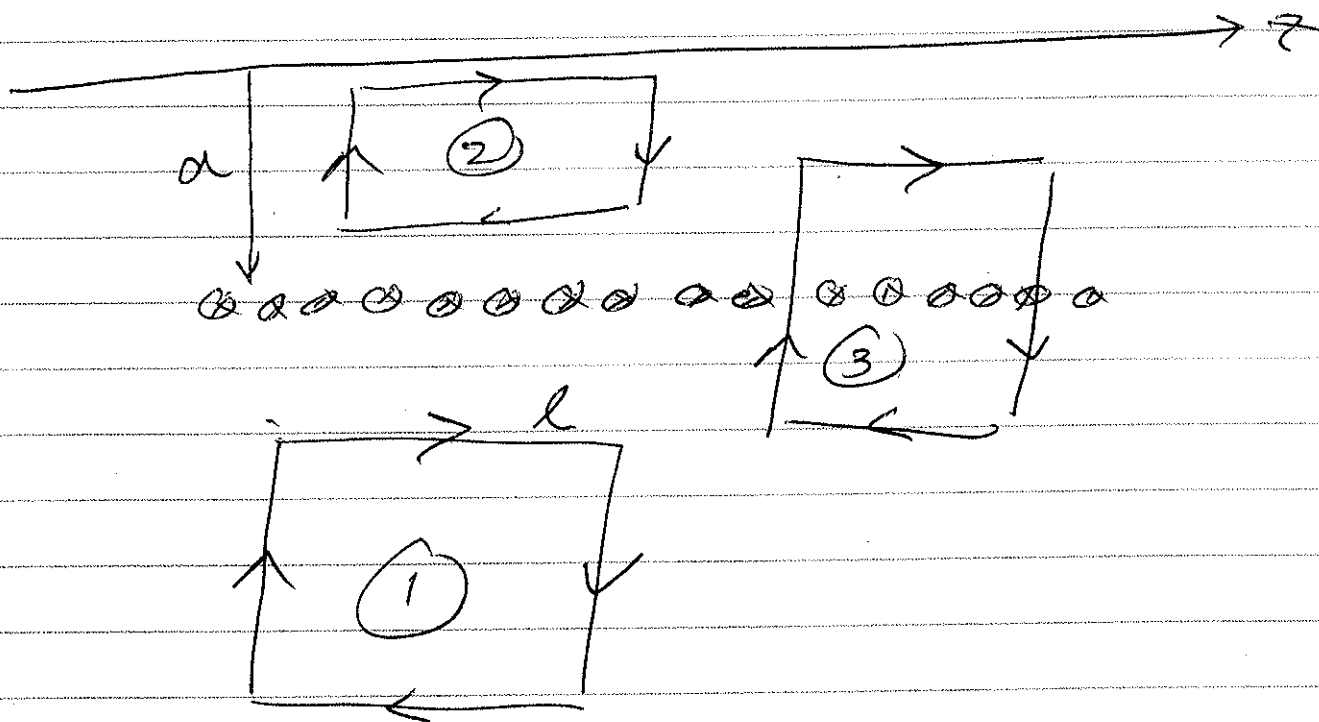
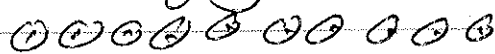
- a)  $N = \#$  of turns per unit length
- b) 2 layers of helical wires w/ opposite pitch  
 $\Rightarrow$  only circular  $I$  sums
- c) Use Ampere's law to find  $\vec{B}$  everywhere and then find  $\vec{A}$ .

d) ~~Biot-Savart law~~  $\Rightarrow B_{\phi} = 0$  because  $I$  is azimuthal.



only way for this to be consistent is if  $B_s = 0$  (b/c  $z=0$  is arbitrary)

$\Rightarrow$  B is going to be in z-direction



$$\textcircled{1} B_{z,out}^1 l + 0 - B_{z,out}^2 l + 0 = \frac{1}{\mu_0} \int \vec{J} \cdot d\vec{S} = 0$$

$0 \text{ at } \infty \Rightarrow B_{z,out} = 0$

$$\Rightarrow B_{z,out}^1 = B_{z,out}^2 \Rightarrow B_{z,out} \text{ is constant for } S > a$$

$$\textcircled{2} B_{z,in}^1 l + 0 - B_{z,in}^2 l + 0 = \mu_0 \int \vec{J} \cdot d\vec{S} = 0$$

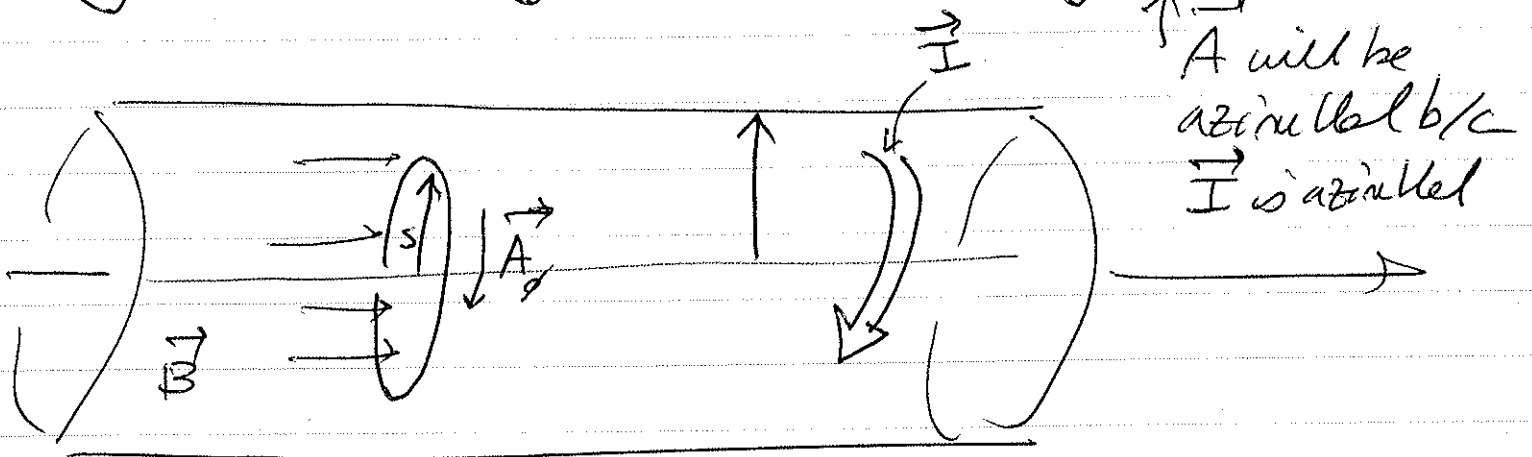
$$\Rightarrow B_{z,in}^1 = B_{z,in}^2 \Rightarrow B_{z,in} \text{ is constant}$$

$$\textcircled{3} B_{z,in} l + 0 - B_{z,out} l = \mu_0 I N l \Rightarrow \underline{B_{z,in} = \mu_0 N I}$$

@ Sol  $\vec{A}$

$$\vec{B} = \nabla \times \vec{A}$$

$$\int \vec{B} \cdot d\vec{S} = \int \nabla \times \vec{A} \cdot d\vec{S} = \oint \vec{A} \cdot d\vec{l}$$



$$a) \int \vec{B} \cdot d\vec{S} = (\mu_0 N I) \pi s^2 = A_{\phi} 2\pi s, \quad s < a$$

$$\Rightarrow A_{\phi} = \frac{\mu_0 N I s}{2} \cdot s < a$$

$$b) \int_0^a \vec{B} \cdot d\vec{S} = (\mu_0 N I) \pi a^2 = A_{\phi} 2\pi s, \quad s > a$$

$$\Rightarrow A_{\phi} = \frac{\mu_0 N I a^2}{2s}, \quad s > a$$

note:  $\vec{B} = 0$  for  $s > a$   
 $\vec{A} \neq 0$  for  $s > a$  } which is "real" field

$$\textcircled{6} (\vec{v} \cdot \vec{A}) = \frac{12}{52} A_x + \frac{12}{52} A_y + \frac{2}{22} A_z$$
$$= 0 + 0 + 0$$

$$\vec{v} \cdot \vec{A} = 0$$