

Electric Conductivity

We have considered dielectrics (where $\vec{P} = \epsilon_0 \chi_e \vec{E}$) and magnetizable media (where $\vec{M} = \chi_m \vec{H}$). Now, let's consider another "electrical" property of matter,
"Conductivity"

(conductivity measured by σ or $\rho = 1/\sigma$). In a conductor there are free charges, and in the presence of a "force" (F , free per unit charge) charges move. That is, we measure

$$\vec{J} = \sigma \left(\frac{\text{Force}}{q} \right) \quad \begin{matrix} \text{actually a "field", force} \\ \text{per unit charge} \end{matrix}$$

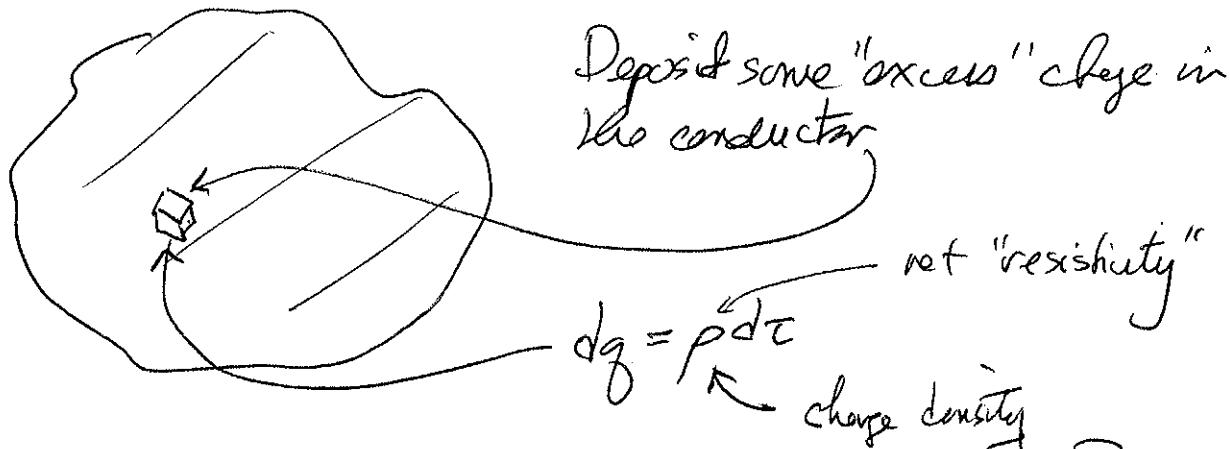
Here, we consider electrical forces and so,

$$\vec{J} = \sigma (\vec{E} + \vec{V} \times \vec{B})$$

or if $|\vec{V} \times \vec{B}| \ll |\vec{E}|$ then

$$\boxed{\vec{J} = \sigma \vec{E}, \text{ "Ohm's law"}}$$

Consider a conductor upto where $\vec{E} = 0$, initially.



Q: How long will this charge excess exist?

"Continuity Equation"

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \vec{J} = 0$$

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\sigma \vec{E}) = 0$$

$$\frac{\partial \rho}{\partial t} + \sigma (\nabla \cdot \vec{E}) = 0$$

$$\frac{\partial \rho}{\partial t} + \sigma \frac{\partial E_x}{\partial x} = 0 \rightarrow \frac{\partial \ln \rho}{\partial t} = -\frac{\sigma}{\epsilon_0}$$



$$\begin{cases} J_x^{\text{out}} \times A = \frac{\Delta Q^{\text{out}}}{S} \\ J_i^{\text{out}} \times A = \frac{\Delta Q^{\text{in}}}{S} \end{cases}$$

$$\rightarrow J_i^{\text{out}} - J_i^{\text{in}} = \frac{\Delta Q}{A \cdot S} \quad \frac{\partial}{\partial t}$$

$$\boxed{\rho = \rho_0 \exp\left(-\frac{\sigma t}{\epsilon_0}\right)}$$

The charge dissipates exponentially. It falls to $1/e^\sigma$ of its size after a time

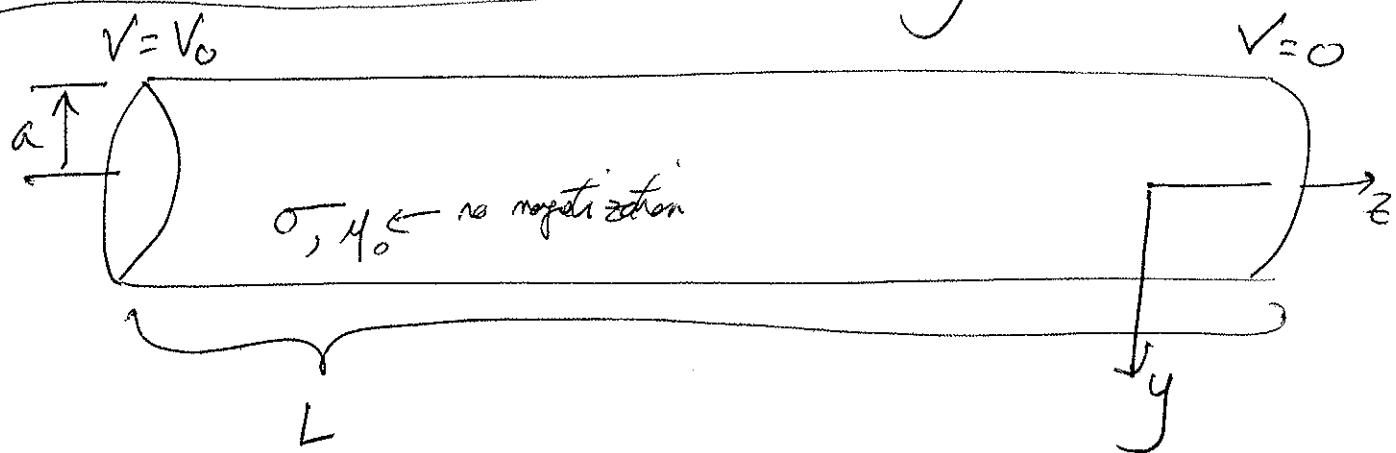
$$\tau_e = \epsilon_0 / \sigma \text{ (e-folding time).}$$

Materials	$\sigma \left(\frac{A}{mV}, (\Omega m)^{-1} \right)$	τ_e
Copper	5.8×10^7	$1.5 \times 10^{19} s$
Germanium	2.2	$4 \times 10^{-12} s$
Glass	$\approx 10^{-12}$	9s
Air	3×10^{-14}	~ 5 minutes

for metals, $\tau_e \ll 1s \Rightarrow \vec{E} = 0$ is rapidly achieved
 (as we inferred (assumed)
 last quarter).

- a) Conductors can very quickly go to equilibrium $\vec{E} = 0$.
- b) No "excess" charge in conductors.
 (can still have currents, however)

Consider a straight wire w/conductivity σ



What are \vec{J} and \vec{B} for this piece of wire?

Because $\vec{J} = \sigma \vec{E}$, we need \vec{E} to find \vec{J} . However, is it as simple as saying

$$\vec{E} = -\frac{\Delta V}{L} \hat{z} = \frac{V_0}{L} \hat{z}?$$

Let's see. We have steady flow

$$(i) \frac{\partial \vec{P}}{\partial t} + \vec{\nabla} \cdot \vec{J} = \vec{\nabla} \cdot \vec{J} = 0 = \vec{\nabla} \cdot (\sigma \vec{E})$$

$$(ii) \text{ steady-state} \Rightarrow \vec{\nabla} \times \vec{E} = 0 \Rightarrow \vec{E} = -\vec{\nabla} V$$

combine (i) and (ii)

$$\vec{\nabla} \cdot \vec{J} = \vec{\nabla} \cdot (\sigma \vec{E}) = -\sigma \vec{\nabla}^2 V = 0$$

$$\Rightarrow \vec{\nabla}^2 V = 0 \quad \text{holds, solve Eqn. later}$$

and the answer ^{is also} as simple as $\vec{E} = \frac{V_0}{L} \hat{z}$!

$$\text{and } V(z) = A' + B'z$$

⑥ at $z=0, V=V_0; z=L, V=0$

$$\Rightarrow A' = V_0, B' = -\frac{V_0}{L}$$

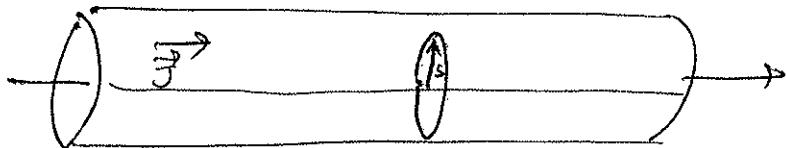
so $\boxed{V(z) = V_0 - \frac{V_0}{L}z} \Rightarrow \boxed{\vec{E} = \hat{z} \frac{V_0}{L}} \checkmark$

The current is then

$$\boxed{\vec{J} = \hat{z} \sigma \frac{V_0}{L}}$$

as guessed ;
hoped for.

\vec{B} can be found from Ampere's law (if $L \gg a$)



$$B_\phi 2\pi s = \mu_0 \int \vec{J} \cdot d\vec{s} = \mu_0 \frac{V_0}{L} \sigma \pi s^2 \quad (\text{inside wire})$$

$$\Rightarrow \boxed{B_\phi = \frac{\mu_0 \sigma V_0 s}{2L} \hat{\phi}}$$

Comment:

$$\begin{aligned} d\vec{F}_B &= \vec{J} \times \vec{B} = -\hat{s} \left[\mu_0 \frac{\sigma^2 V_0}{2L^2} s \right] d\vec{l} \\ &= -\hat{s} \left[\mu_0 \frac{\sigma^2 V_0}{2L^2} s \right] s ds d\phi L \end{aligned}$$

$$\left\{ \vec{F}_B \right\} = -\hat{s} \left(\mu_0 \frac{\pi \sigma^2 V_0}{3L^2} a^3 \right); \text{ why doesn't wire collapse?}$$

Ohm's Law

Let's return to $\vec{J} = \sigma \vec{E}$ and re-write this in a more familiar way

$$\text{a) } \vec{J} = \sigma \vec{E}$$
$$z \left(\frac{I}{A} \right) \quad \left[\frac{V_0}{L} \right] \hat{z}$$
$$\Rightarrow V_0 = \left(\frac{L}{\sigma A} \right) I$$

$R = \text{resistance} \Rightarrow$

$$z \left[\frac{L}{\sigma A} \right]$$

$$V = IR$$

"Ohm's" law

geometric quantities
+ σ

Ohmic losses, Joule Heat, Power

Recall: $\vec{J} = \sigma \vec{E} = \text{constant for steady current}$

however, $m\ddot{\vec{z}} = q(\vec{E} \cdot \vec{z}) \Rightarrow \ddot{\vec{z}} \neq 0$
 $\rightarrow \text{constant acceleration?}$

Recall, on a volume, we have the force micro vs macro vs diff

$$\Delta \vec{F} = \int [P_{\text{micro}} \vec{E}_{\text{macro}} + \vec{J}_{\text{macro}} \times \vec{B}_{\text{macro}}] dV$$

where $P_{\text{micro}} = P_{\text{ave}} + \delta P$ (i) "wave" are macroscopic properties
 $\vec{E}_{\text{micro}} = \vec{E}_{\text{ave}} + \delta \vec{E}$
 $\vec{J}_{\text{micro}} = \vec{J}_{\text{ave}} + \delta \vec{J}$ (ii) "f" are fluctuations
 $\vec{B}_{\text{micro}} = \vec{B}_{\text{ave}} + \delta \vec{B}$

1st order terms average to 0 over the adiabatic nutcycles

$$\begin{aligned} \Rightarrow \Delta \vec{F} &= \int [P_{\text{ave}} \vec{E}_{\text{ave}} + \vec{J}_{\text{ave}} \times \vec{B}_{\text{ave}}] dV + \int [\delta P \delta \vec{E} + \delta \vec{J} \times \delta \vec{B}] dV \\ &= [P_{\text{ave}} \vec{E}_{\text{ave}} + \vec{J}_{\text{ave}} \times \vec{B}_{\text{ave}}] dV + \int [\delta P \delta \vec{E} + \delta \vec{J} \times \delta \vec{B}] dV \end{aligned}$$

power delivered to the charges by "battery"

\Rightarrow acceleration

collisions between particles dissipate "energy" "heat"

\Rightarrow drag

Lof's return to chronic losses (consider Work)

$$dW_i = g_i \vec{E}_{\text{micro}} \cdot d\vec{r}_i$$

For a system of charges, the rate at which work is performed is

$$\frac{dW_i}{dt} = g_i \cdot \vec{E}_{\text{micro}} \cdot \vec{dr_i} = \text{Power} = P$$

$$\frac{d\vec{W}_c}{dt} = \sum_i g_i \vec{E}_{\text{micro}} \cdot \vec{V}_i \quad \leftarrow \text{Work done by collection of } \vec{J}_i \text{ charges}$$

Consider a collection of loops that can be treated as averages

$$\cancel{P_{\text{micro}} = \sum_i g_i(t) \Rightarrow P_{\text{micro}} = P_{\text{ave}} + \delta P}$$

not

$$\cancel{g_i(t) = [P_{\text{ave}} + \delta p] [V_i + \delta V]} \quad \cancel{3}$$

$$\cancel{= [P_{\text{ave}} + \delta p] \delta V} \quad \cancel{3}$$

$$\Rightarrow \frac{dW_i}{dt} = \int (\vec{J}_{ave} + d\vec{J}) \cdot (\vec{E}_{ave} + d\vec{E}) d^3x$$




$\int \vec{J}^+ \cdot d\vec{x}$ order has integrate to 0 one time & space

$$\frac{dW_i}{dt} = \int \left[\vec{J}_{ave} \cdot \vec{E}_{ave} + d\vec{J} \cdot d\vec{E} \right] d^3x = P$$

Integrate over a volume ΔV

$$\Rightarrow \Delta P = \underbrace{\vec{J}_{ave} \cdot \vec{E}_{ave}}_{\text{power stored by battery to charges}} \Delta V + \underbrace{\int d\vec{J} \cdot d\vec{E} d^3x}_{\Delta V} \quad \text{in other's power absorbed by electron carriers (e^-'s) and background ions}$$

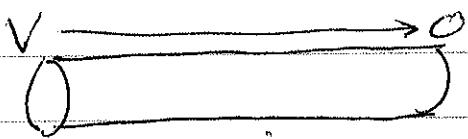
power stored by battery to charges

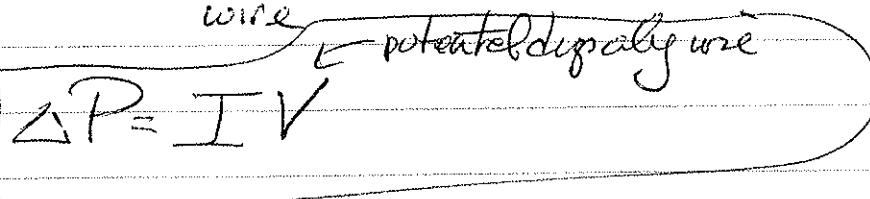
in other's power absorbed by electron carriers (e^-'s) and background ions

$$\boxed{\Delta P = \vec{J}_{ave} \cdot \vec{E}_{ave} \Delta V}$$

$$\text{For a uniform wire } \boxed{\vec{J}_{ave} dV = I d\vec{l}}$$

$$\Rightarrow \Delta P = \int \vec{I} d\vec{l} \cdot \vec{E}_{ave} = I \underbrace{\int \vec{E}_{ave} d\vec{l}}_{\Delta V} = -IV$$

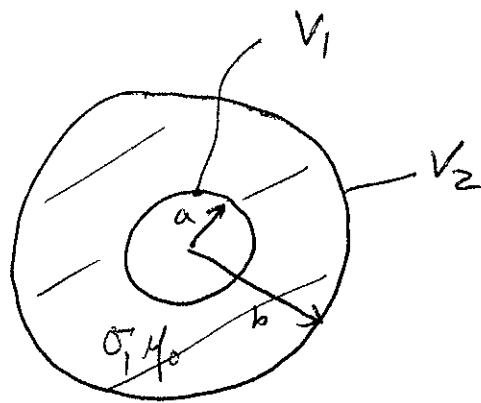
note:  , $\Delta V = 0 - V$

and  $\Delta P = IV$

(HW)
Example 2 Prob. 7.1

2 concentric spheres ad
the region between is
filled w/ a material w/
conductivity σ .

$\Delta V = V_0$. What are I and R ?



Sol^a Steady-state & uniform $\sigma \Rightarrow \nabla^2 V = 0$

$$\Rightarrow V = D - C/r \quad \left\{ \begin{array}{l} \text{as solution of Laplace eqn. in} \\ \text{spherical polar coordinates} \end{array} \right.$$

a) Apply BC's

$$\left\{ \begin{array}{l} r=a \Rightarrow V_1 = D - C/a \\ r=b \Rightarrow V_2 = D - C/b \end{array} \right.$$

$$\Rightarrow V_1 + \frac{C}{a} = V_2 + \frac{C}{b} \Rightarrow$$

$$C = \frac{V_2 - V_1}{\frac{1}{a} - \frac{1}{b}}$$

and

$$D = V_1 + \frac{b}{b-a} (V_2 - V_1)$$

b) $V = D - C/r$

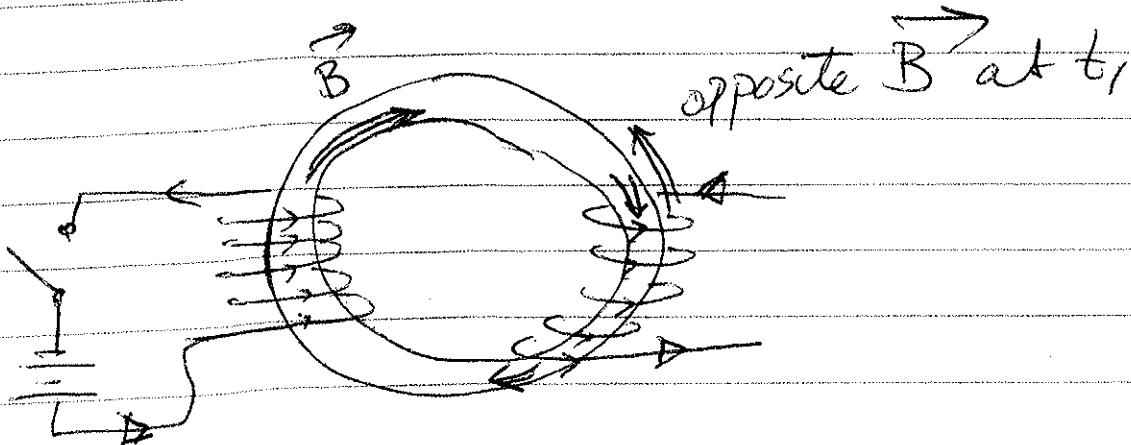
$$\vec{E} = \hat{r} (C/r^2) = \frac{ab}{b-a} (\underbrace{V_2 - V_1}_{\Delta V = V_0}) \hat{r} \frac{1}{r^2}$$

$$\Rightarrow \vec{J} = \sigma \vec{E}_r = \sigma V_0 \frac{ab}{b-a} \frac{\hat{r}}{r^2}$$

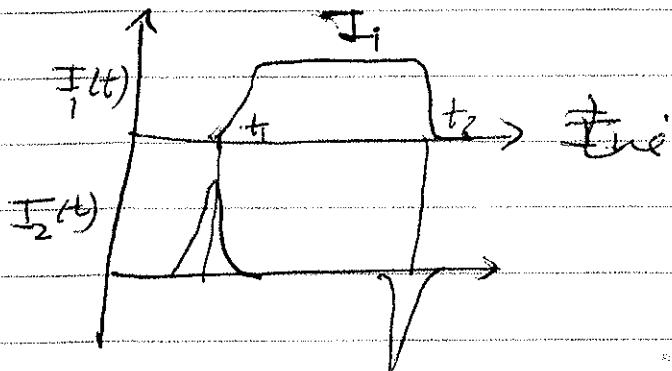
E-fields from Time-Varying \vec{B} fields

1820 $\rightarrow I \rightarrow \vec{B}$

1831 \rightarrow Faraday (t Henry) said let $\vec{B} \Rightarrow \vec{E}$



close switch
→ I flows
as shown



Current flows to make \vec{B} & $\oint_B \vec{B} \cdot d\vec{s} = 0$
day exposed

Lenz's Rule: the sense of the induced current (induced EMF) is to oppose the change in magnetic flux, Φ

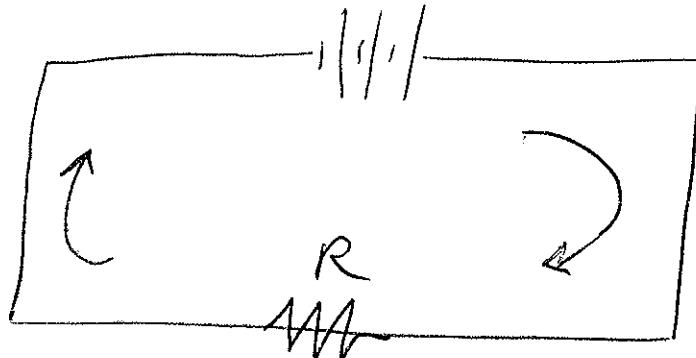
Faraday said let $E = IR = -\frac{d}{dt} \Phi_B$

Electromotive force (E , emf)

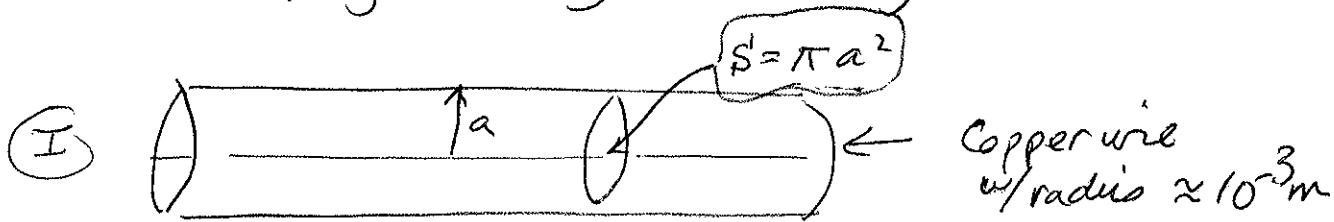
Voltage difference
across some
element of a
"circuit".

Consider

V , potential across terminals



- ① Battery supplies a "push" right around itself.
However, lights go essentially right after you "flick" the switch. Can we expect that this is due to e^-' s being around by the battery?



We have $\vec{J} = (n_e e) \vec{V}_e$
charge density

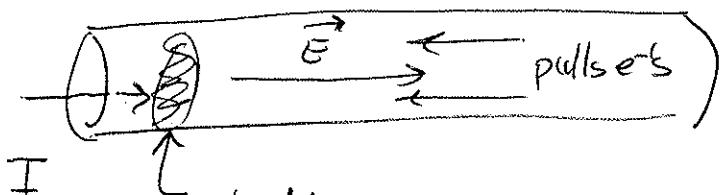
$$\Rightarrow \vec{J} d\tau = I d\vec{l} \Rightarrow I d\vec{l} = e n_e \vec{V}_e d\tau$$

and $V_e = \frac{I d\tau}{e n_e d\tau} = \frac{I}{e n_e S}$ ← 1 Amp
 $S = \text{area}$
 $8.5 \times 10^{28} \text{ m}^{-3}$

$\boxed{V_e \approx 10^{-4} \frac{\text{m}}{\text{s}}}$

\Rightarrow takes too long for e⁻'s to supply push directly

(4)



I

charge builds up

$\Rightarrow \vec{E}$ gets steeper

up essentially instantaneously ($c = \text{signal speed}$)

\Rightarrow ad \vec{E} gets erased on the light-tavel time
(essentially).

\Rightarrow two "forces" act on wire, battery + $\vec{E}^{\text{(induced)}}$

fields: $\vec{f} = \vec{f}_s + \delta \vec{E}$

\vec{f}_s $\vec{\delta E}$

(induced + fluctuations)

battery

microscopic in origin, net like
macroscopic applied

(macroscopic applied field)

field (but is actually
fluctuating field +
induced field)

= In our language

"The emf (E) is the work done for each unit of charge transferred around the circuit."

$\Rightarrow E = \oint \vec{f} \cdot d\vec{r} \Rightarrow = - \frac{d}{dt} \Phi_B$

Faraday's Observation

"formal" definition

Onto Maxwell's Equations

Structures

Consider some \mathcal{E} 's (emf's) -- "Microscopic \mathcal{E} 's"

(A) Resistive emf (microscopic)

$$\mathcal{E} = \int_a^b \delta \vec{E}_\text{micro} \cdot d\vec{r}$$

Structuring part of \vec{E}_micro

$$= \int_a^b (\vec{E}_\text{micro} - \vec{E}) \cdot d\vec{r}$$

$d\vec{r}$, m average

Because charges do not accelerate, $\int_a^b \vec{E}_\text{micro} \cdot d\vec{r} = 0$

no net work performed

$$\mathcal{E} = - \int_a^b \vec{E} \cdot d\vec{r}$$

Ohm's law

Resistive emf,

$$\mathcal{E} = - \int_a^b \frac{\vec{J}}{\sigma} \cdot d\vec{r} = - \frac{I}{\sigma A} (b-a)$$

recall: this is R

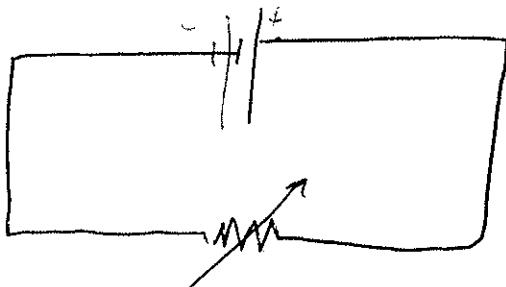
$$\boxed{\mathcal{E}_R = -RI}$$

(B) Battery emf

$$\mathcal{E}_\text{battery} = V \quad \text{for } I = 0 \quad (f = 0 \text{ because } \sigma \rightarrow \infty)$$

$\rightarrow \delta E = -f_s$

Prob. 7.5
Example



$V_b = r$ not an ideal battery

Voltage across the terminals of the battery

$$V = (E - Ir) = IR$$

variable resistor

To deliver the maximum possible "load" to the resistor, what should R be?

(i) "Load" = Power = $IV = I^2R$ should be maximized

$$\Rightarrow 0 = E - \left(\frac{P}{R}\right)^{\frac{1}{2}}r - \left(\frac{P}{R}\right)^{\frac{1}{2}}R$$

$$P^{\frac{1}{2}}R + P^{\frac{1}{2}}r + (E -)R^{\frac{1}{2}} = 0$$

$$P^{\frac{1}{2}} = \frac{(E -)}{(r+R)} R^{\frac{1}{2}}$$

$$P = \frac{(E -)^2 R}{(r+R)^2}$$

$$\frac{dP}{dR} = \frac{(E -)^2}{(r+R)^2} - \frac{2(E -)^2}{(r+R)^3} R$$

= 0, for extrema

$$\Rightarrow (E -)^2(r+R) = 2(E -)^2 R$$

$$\Rightarrow R = r$$

batteries, ad
so on...

$$\vec{F} = \vec{f}_S + (\delta \vec{E}, \delta \vec{B})$$

Induction \mathcal{E} (emf) \leftarrow Macroscopic forces

a) $\mathcal{E} = \oint \vec{f} \cdot d\vec{r} = \oint (\vec{E} + \vec{V}_e \times \vec{B}) \cdot d\vec{r}$

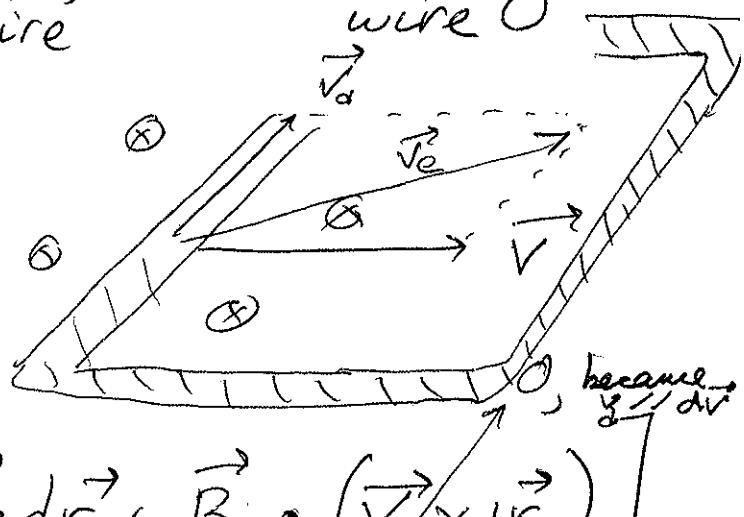
$d\vec{r}$ along wire

line integral along wire

$$V_e \equiv \text{Electron } \vec{v} = \vec{v} + \vec{v}_d$$

\vec{v} motion of wire
 \vec{v}_d drift along wire

$$\mathcal{E} = \oint [\vec{E} \cdot d\vec{r} + \vec{V}_e \times \vec{B} \cdot d\vec{r} + \vec{v}_d \times \vec{B} \cdot d\vec{r}]$$



$$= \oint [\vec{E} \cdot d\vec{r} + \vec{V} \times \vec{B} \cdot d\vec{r} + \vec{B} \cdot (\vec{v} \times d\vec{r})]$$

$\mathcal{E} = \oint [\vec{E} \cdot d\vec{r} + \vec{V} \times \vec{B} \cdot d\vec{r}]$

\vec{v} of wire!

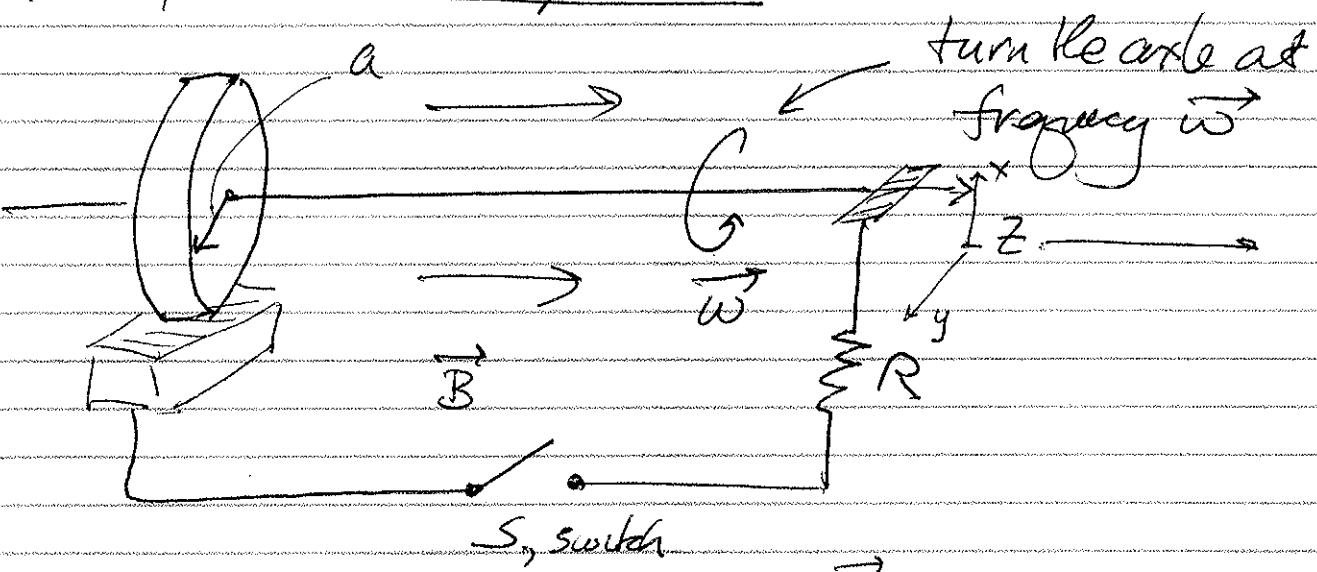
recall, $d\vec{r}$ along wire

Empirically, Faraday found that

$$\mathcal{E} = - \frac{d}{dt} \Phi_B = - \frac{d}{dt} \int \vec{B} \cdot d\vec{S}$$

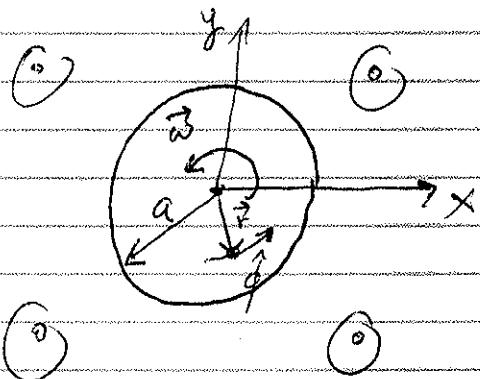
recall (Φ_B)

Homopolar Generator/Motor



a) If S is open (E_f)

$$E = \int (\vec{V} \times \vec{B}) \cdot d\vec{l}$$



$$\vec{v} = \vec{\omega} \times \vec{r} = \omega r \hat{\phi} \Rightarrow \vec{\omega} \times \vec{B} = \omega r \hat{\phi} \times \vec{B}$$

$$E = \int (wr\hat{\phi} \times B_0 \hat{z}) \cdot d\vec{r}$$

$$= \frac{\omega r^2 B_0}{2} \Big|_0^a \text{ subtract}$$

$$\boxed{E = \frac{1}{2} \omega B_0 a^2}$$

b) Close S $\Rightarrow E = IR \rightarrow \frac{1}{2} \omega B_0 a^2 = IR$

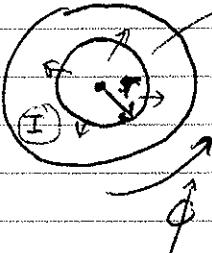
$$\boxed{I = \frac{\omega B_0 a^2}{2R}}$$

c) The current I back-reacts on the wheel.
 Find the induced torque and power needed
 to power the generator.

$$(i) \vec{I} = \frac{\omega B_0 a^2}{2R} \hat{r} \Rightarrow \text{force}$$

$$Idr \vec{r} = K ds$$

$$K = \left(\frac{I}{2\pi r} \right) \hat{r} \Rightarrow dF = K ds \times \vec{B}$$

$$= \frac{IB_0}{2\pi r} (radr) (-\hat{z})$$


$$(ii) \text{Torque, } dN = \vec{r} \times dF = \frac{IB_0}{2\pi} dr dr (-\hat{z})$$

$$\Rightarrow N = \int \frac{IB_0}{2\pi} r dr dr (-\hat{z})$$

$$= \int \left(\frac{\omega B_0 a^2}{2R} \right) \left(\frac{B_0}{2\pi} \right) [r dr dr] (-\hat{z})$$

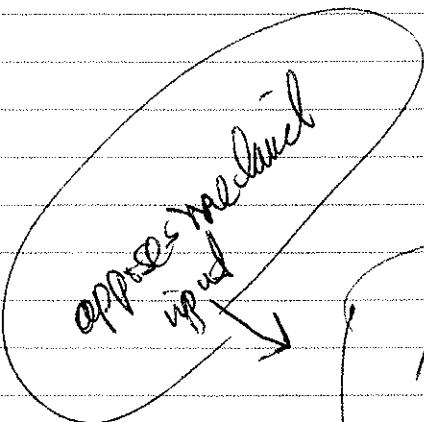
$$= \frac{\omega B_0^2 a^2}{2R} \left(\frac{B_0}{2\pi} \right) \left(\frac{r^2}{2} \right) \Big|_0^a (-\hat{z})$$

$$N = \frac{\omega B_0^2 a^4}{4R} (-\hat{z})$$

"we" must supply
this mechanical
effort to maintain

$$\vec{\omega}$$

Opposes $\vec{\omega}$



$$(iii) W = \int_0^\phi \vec{N} \cdot d\vec{\phi}^1 \quad \text{to turn from } \phi=0 \rightarrow \phi$$

$$= \frac{\omega B_0 a^4}{4R} \phi$$

Power is the rate of work $\Rightarrow \dot{\phi} = \phi/t = \omega$

$$\Rightarrow \frac{dW}{dt} = P = \frac{\omega^2 B_0 a^4}{4R}$$

We supply this power to keep the wheel going at constant a

find Chassis losses (load)

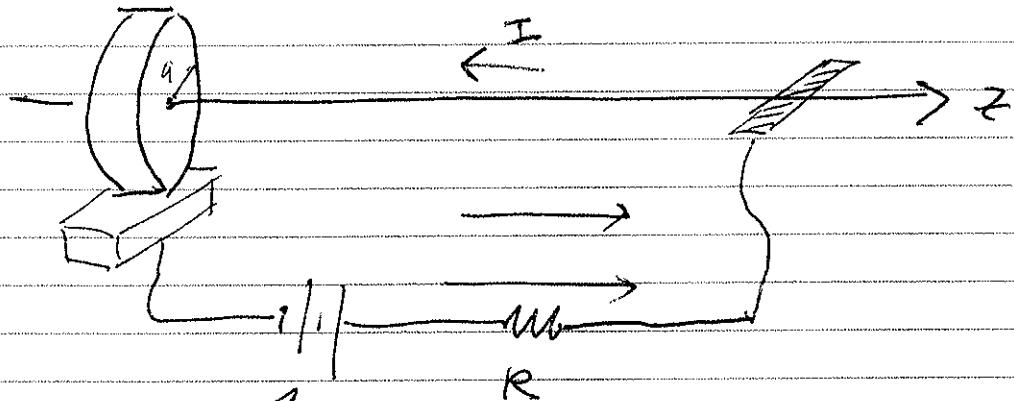
$$I = \frac{\omega B_0 a^2}{2R} \Rightarrow I = \frac{\omega^2 B_0 a^4}{4R^2} = \frac{P}{R}$$

$$\Rightarrow P_{losses} = I^2 R$$

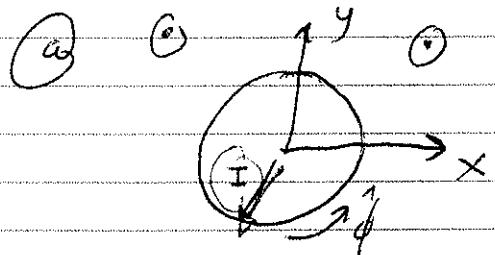
\uparrow
Some as input power

Motor

$$\vec{B} = B_0 \hat{z}$$



$$\text{Battery, } V \Rightarrow V = IR \rightarrow I = V/R$$



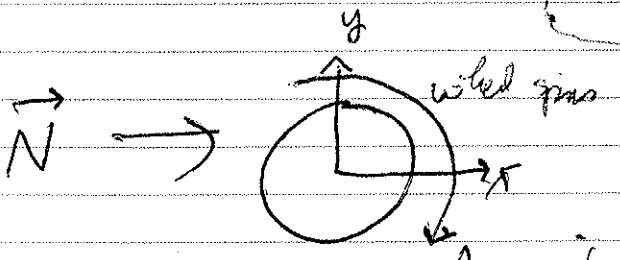
$$d\vec{F} = \left(\frac{I}{2\pi r}\right) \hat{r} (rd\phi dr) \times B_0 \hat{z}$$

$$\vec{F} = I r B_0 \int_a^a (-\dot{\phi}) ; \text{ total force}$$

we are interested in torque

$$d\vec{N} = \vec{r} \times d\vec{F} = r \left(\frac{I}{r}\right) r dr B_0 (-\hat{z})$$

$$\Rightarrow \vec{N}_z = \frac{Ia^2 B_0}{2} \hat{z} = -\frac{Va^2 B_0}{2R} \hat{z}$$



"locked" rotor torque (torque when $\vec{\omega} = 0$)

(b) as $\omega \uparrow \Rightarrow$ a back-reaction occurs \Rightarrow "drag"

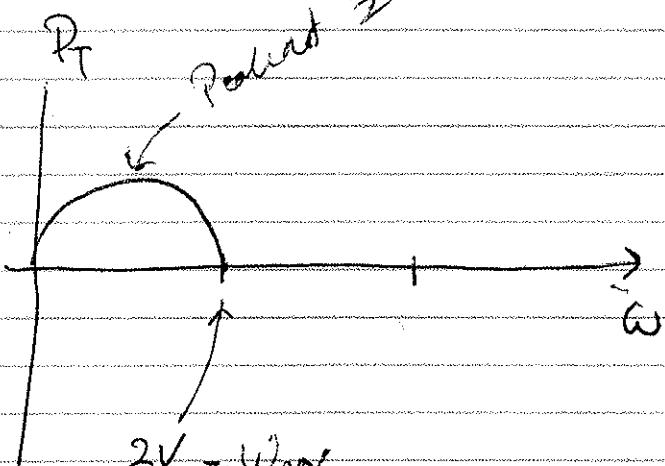
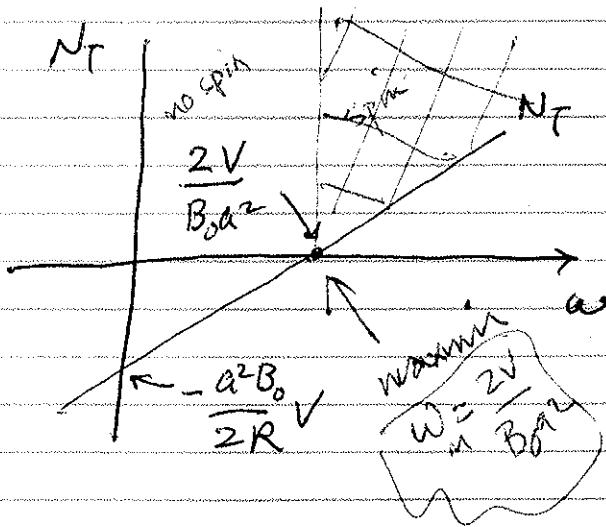
$$\omega \Rightarrow \vec{N}_b = \frac{\omega B_0^2 a^4}{4R} \hat{z} \text{ from (generator)}$$

(c) Total torque as a function of ω

$$\vec{N}_T = \vec{N} + \vec{N}_b = \left[\frac{Va^2 B_0}{2R} + \frac{\omega B_0^2 a^4}{4R} \right] \hat{z}$$

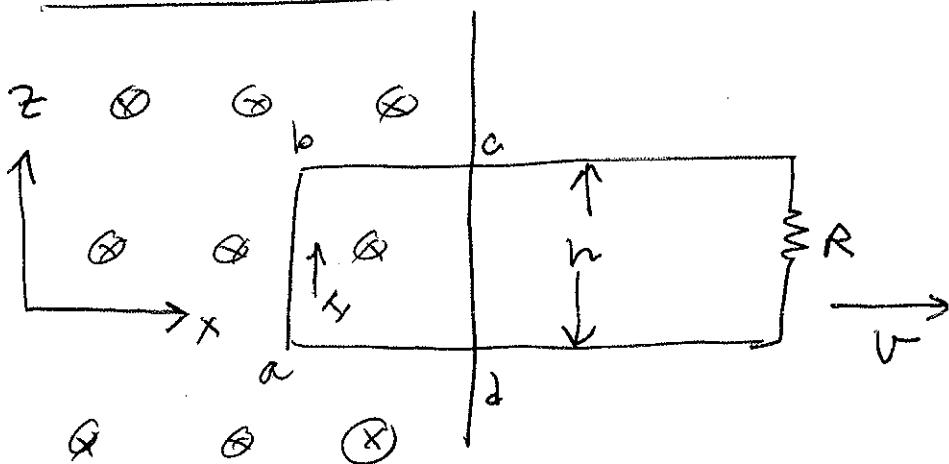
$$= -\frac{Va^2 B_0}{2R} \sqrt{1 - \frac{B_0 a^2}{2V} \omega} \hat{z}$$

$$P_T = \frac{Va^2 B_0}{2R} \sqrt{1 - \frac{B_0 a^2}{2V} \omega} \omega$$



$$\frac{dP_T}{d\omega} = \frac{Va^2 B_0}{2R} \left\{ 1 - \frac{B_0 a^2}{2V} \omega \right\}$$

Motional Emf



What is the force on the moving loop?

$$\vec{F} = q\vec{v} \times \vec{B} = qvB\hat{z}$$

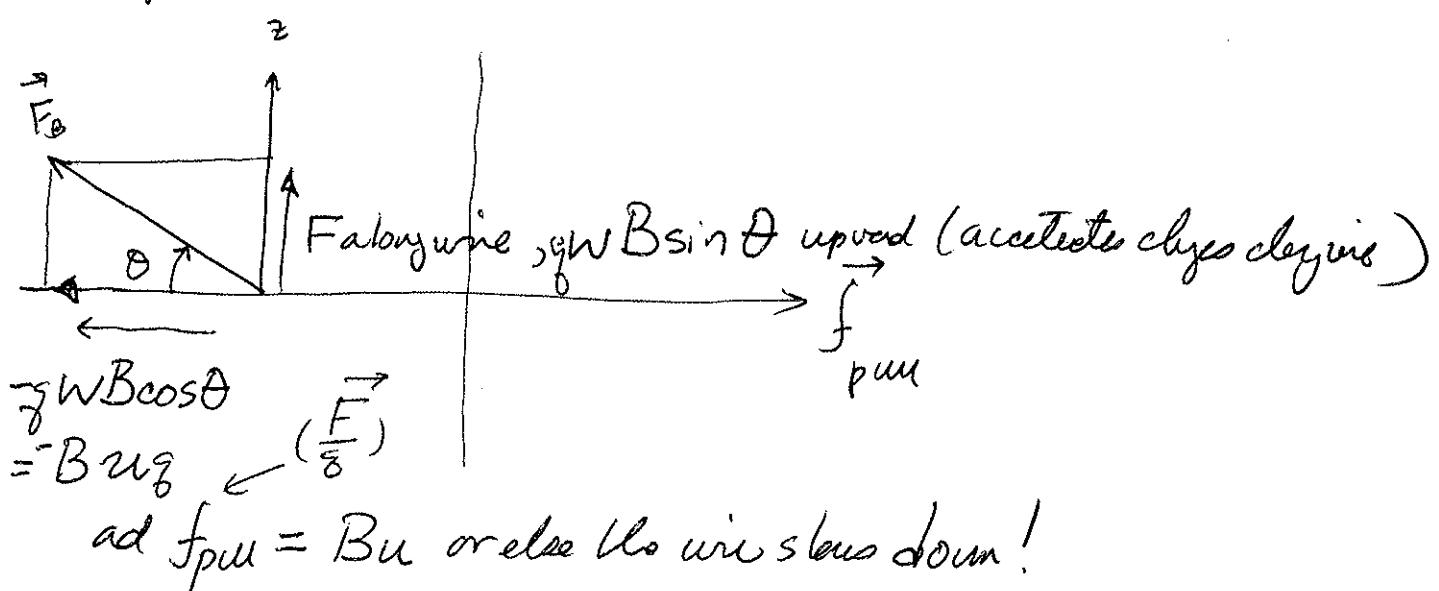
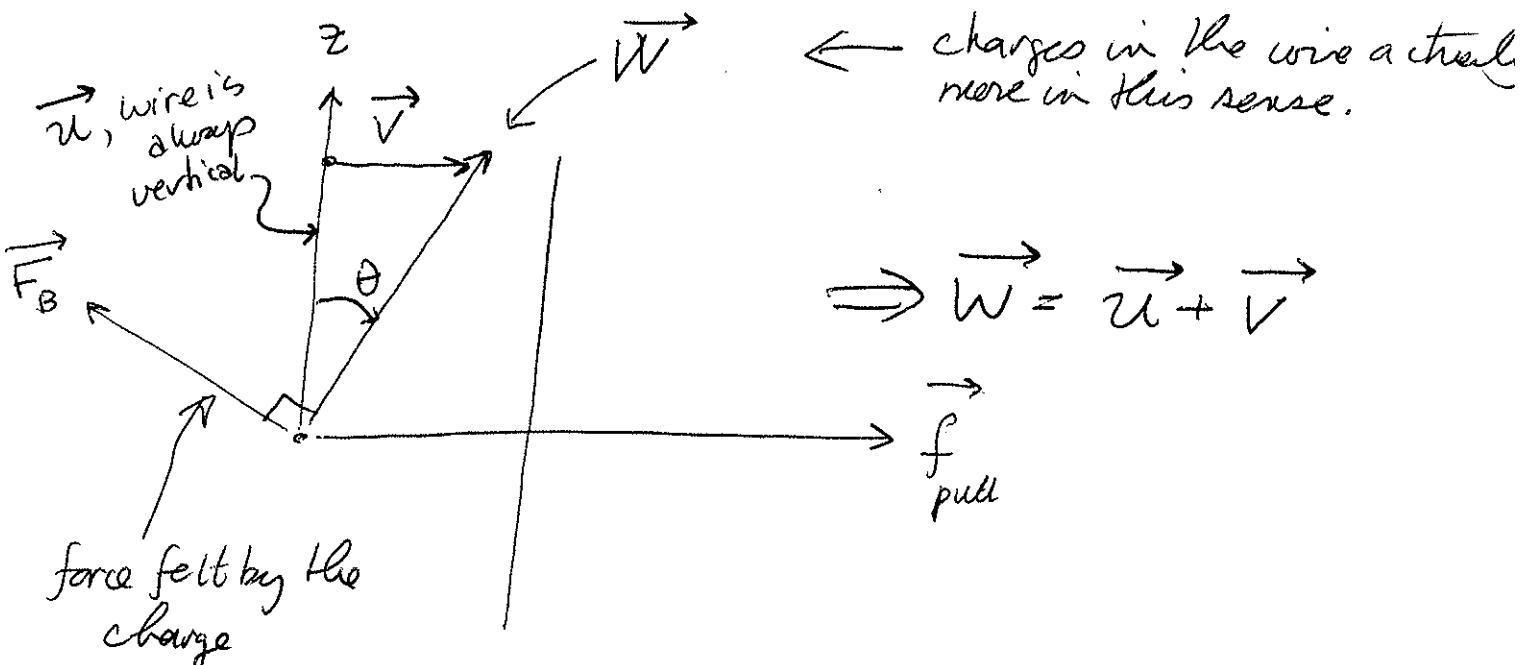
What is the induced emf?

$$\begin{aligned} \text{Emf} &= \oint \vec{f} \cdot d\vec{l} = \oint \left(\frac{\vec{F}}{q} \right) \cdot d\vec{l} = \oint (\vec{v} \times \vec{B}) \cdot d\vec{l} \\ &= Bv \int \hat{z} \cdot d\vec{l} + \dots \end{aligned}$$

$$\boxed{\text{emf} = Bvh}$$

Question: What is the origin of this energy?
B fields do no work.

(See page 295-296 in text)



What is the "emf" due to this force?

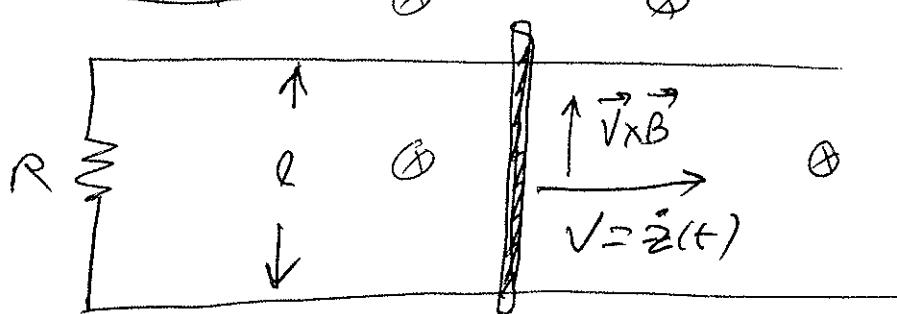
$$\int \vec{f}_{\text{pull}} \cdot d\vec{l} = \sin \theta Bu \left(\frac{h}{\cos \theta} \right) = \underbrace{u \tan \theta}_{} Bh$$

$$= V Bh$$

\cong Motional emf

\Rightarrow whatever pulls the wire, does the work!
(it is not the B-field)

Prob 7.7 (Hw)



A metal bar of mass m slides on two rails a distance l apart. A resistor R is connected across the rails and a uniform \vec{B} points out the page. The bar moves to the right at speed v .

a) $\frac{\text{Find } I}{\text{Emf}} = \oint (\vec{V} \times \vec{B}) \cdot d\vec{l} = VBl$

$$\text{Emf} = IR \rightarrow I = \frac{VBl}{R}; \text{ ccw}$$

b) $\vec{F}_B = g(\vec{V} \times \vec{B}) \uparrow \text{ if } g > 0$

c) find $\ddot{z}(t)$

$$m_b \ddot{z}(t) = \oint I d\vec{l} \times \vec{B} = -I l B$$

$$= -\frac{Bl}{R} \dot{z} l B$$

$$= -\frac{B^2 l^2}{R} \dot{z}$$

$$\Rightarrow \ddot{z} + \left(\frac{B^2 l^2}{m_b R} \right) \dot{z} = 0$$

$$\boxed{\dot{z}(t) = -\left(\frac{B^2 l^2}{m_b R} \right) z(t) + \dot{z}_0}$$

Faraday's Observation,

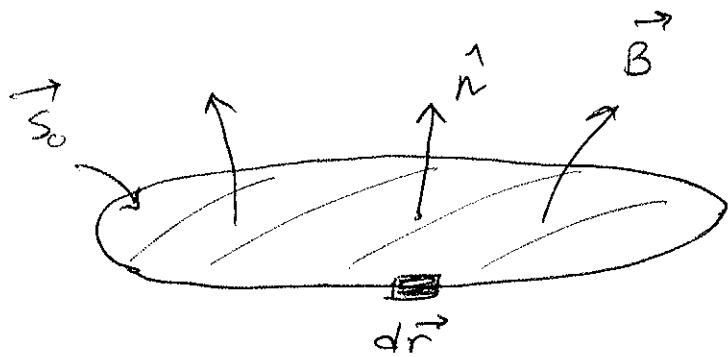
$$\mathcal{E} = -\frac{d}{dt} \oint_B$$

and so,

$$\begin{aligned} \mathcal{E} &= \oint [E + \vec{v} \times \vec{B}] \cdot d\vec{r} = -\frac{d}{dt} \int \vec{B} \cdot d\vec{S} \\ &\quad \left. \begin{array}{l} \text{defn} \\ \text{Motional Emf} \end{array} \right\} \quad \left. \begin{array}{l} \text{Faraday} \\ \text{loop changes} \end{array} \right\} \quad \left. \begin{array}{l} \text{time-varying} \\ \vec{B} \\ \vec{B} \text{ independent of} \\ \text{time} \end{array} \right\} \\ &= -\frac{d}{dt} \int d\vec{S} \cdot \vec{B} - \int \frac{\partial \vec{B}}{\partial t} \cdot d\vec{S} \\ &= -\frac{d}{dt} \oint_B^C - \frac{d}{dt} \oint_B^B \end{aligned}$$

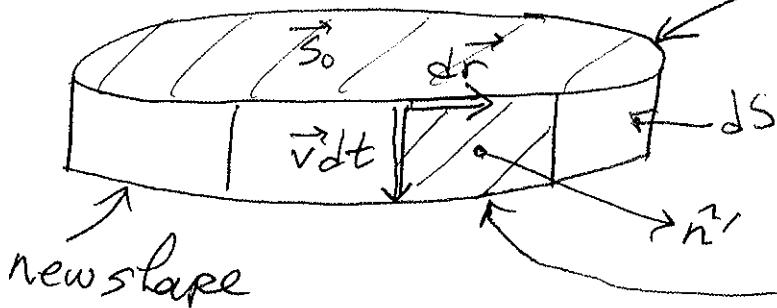
Look at \oint_B terms in more detail

(i) $\vec{B} = 0 \Rightarrow$ time-independent \vec{B}

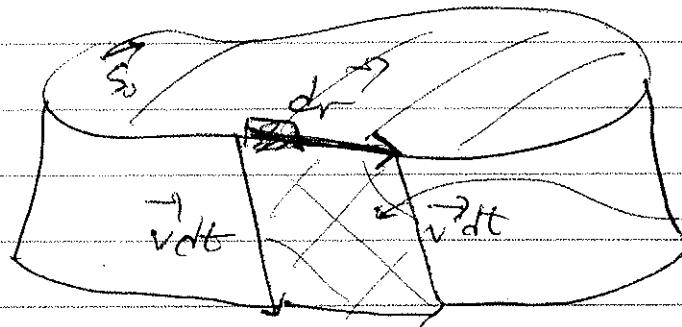


$$\begin{aligned} &\text{at time } t=0 \\ &\Rightarrow \oint_B = \int \vec{B} \cdot d\vec{S} \end{aligned}$$

at time $t=t>0$, if $\vec{v} \neq 0$ shape of circuit at $t=0$

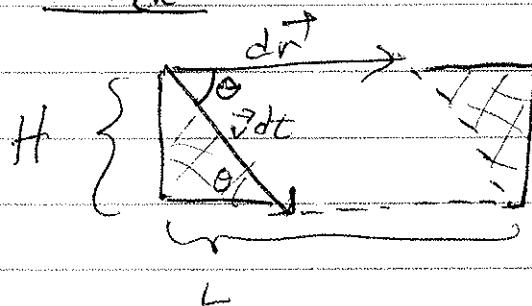


for small dt , new area is
 $\vec{S}_0 + d\vec{S}$
 what is $d\vec{S}$?



We want to see how the area changes because of the motion of the circuit.

Consider



a) make the parallelogram as shown

b) add the triangles to make it a rectangle

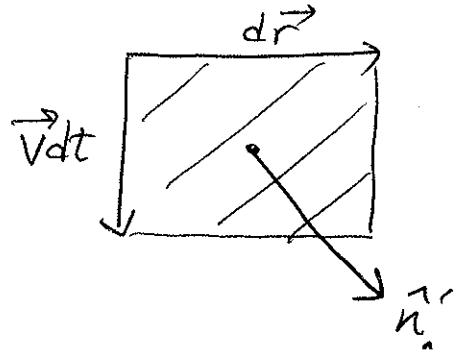
$$\text{Area of Rectangle} = LH = (\underbrace{dr + vdt \cos\theta}_{\text{width}}) \times (vdt \sin\theta)$$

$$= \boxed{\text{rectangle}} + 2 \left[\underbrace{\frac{1}{2} (vdt \cos\theta) vdt \sin\theta}_{\text{2 triangles area of triangle}} \right]$$

$$\Rightarrow \boxed{\text{rectangle}} = vdt dr \sin\theta$$

$$\Rightarrow \boxed{d\vec{S} = \vec{v} dt \times \vec{dr}}$$

The change in the area $d\vec{S}$ is then



$$d\vec{S} = (\vec{V}dt \times d\vec{r})$$

$$\hat{n}'dS = \vec{V}dt \times d\vec{r}$$

The change $d\dot{\Phi}_B^c$ is then

$$d\dot{\Phi}_B^c = \vec{B} \cdot d\vec{S} = \vec{B} \cdot (\vec{V}dt \times d\vec{r})$$

The total change in $\dot{\Phi}_B^c$ is then

$$\begin{aligned} \frac{d\dot{\Phi}_B^c}{dt} &= \oint \vec{B} \cdot (\vec{V} \times d\vec{r}) \\ &= \oint (\vec{B} \times \vec{V}) \cdot d\vec{r} \end{aligned}$$

exchange "dot" and "cross"

$$\boxed{\frac{d\dot{\Phi}_B^c}{dt} = -\oint (\vec{V} \times \vec{B}) \cdot d\vec{r}}$$

$\frac{F_{\text{Lorentz}}}{q}$

Okay, so the emf due to the motion of the circuit is the "walk" alone by the $(\vec{V} \times \vec{B})$ force!

Fromm, so this now flat

$$\oint [E \cdot d\vec{r} + (\vec{v} \times \vec{B}) \cdot d\vec{r}] = - \frac{d\Phi_B^i}{dt} - \frac{d\Phi_B^B}{dt}$$

$$\Rightarrow \oint E \cdot d\vec{r} = - \frac{d\Phi_B^B}{dt} = - \int \frac{\partial \vec{B}}{\partial t} \cdot d\vec{S}$$

a time-varying \vec{B} -field induces an electric field!

Use Stokes's theorem to convert the line integral to a surface integral,

$$\oint E \cdot d\vec{r} = \int (\nabla \times E) \cdot d\vec{S} = - \int \frac{\partial \vec{B}}{\partial t} \cdot d\vec{S}$$

$$\int [\nabla \times E + \frac{\partial \vec{B}}{\partial t}] \cdot d\vec{S} = 0$$

for arbitrary $d\vec{S}$

$$\Rightarrow \boxed{\nabla \times E = - \frac{\partial \vec{B}}{\partial t}}$$

Faraday's law in differential form for the varying fields

Currently Maxwell Equations

$$\vec{\nabla} \cdot \vec{E} = \rho/\epsilon_0$$

$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$$

Amper's law (law basically as
is only seen from static
current and "fictitious" (flux))

$$\boxed{\text{Ampere's law: } \nabla \times \vec{B} = \mu_0 \vec{J}}$$

Further

$$C = \frac{Q}{V} a \Rightarrow V = \frac{Q}{C} + IR$$

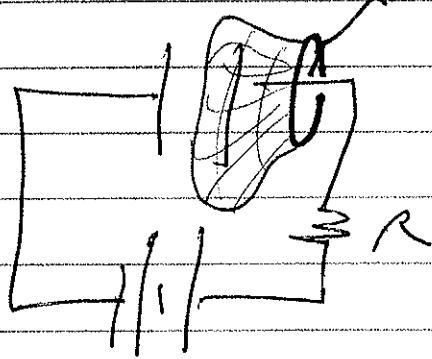
$$E_b = \frac{Q}{C} + R \frac{dQ}{dt}$$

$$\oint \vec{B} \cdot d\vec{l} = \mu_0 \int \vec{J} \cdot d\vec{s}$$

$$= \mu_0 I$$

C

Sur surface as
slab



$$\oint \vec{B} \cdot d\vec{l} = \mu_0 \int \vec{J} \cdot d\vec{s}$$

$$= 0 !$$

V

Sur surface as
slab

$$\nabla \times \vec{B} = \mu_0 \vec{J}$$

has issues

$$\Rightarrow \nabla \cdot \left[\vec{V} \times \vec{B} - \mu_0 \left(\vec{J} + \epsilon_0 \frac{\partial \vec{E}}{\partial t} \right) \right] = 0$$

or $\vec{V} \times \vec{B} = \mu_0 \vec{J} + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t}$

displacement current

Maxwell Equations

$$\vec{V} \cdot \vec{E} = \rho \epsilon_0$$

$$\vec{V} \cdot \vec{B} = 0$$

$$\vec{V} \times \vec{E} = - \frac{\partial \vec{B}}{\partial t}$$

$$\vec{V} \times \vec{B} = \mu_0 \vec{J} + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t}$$

Suppose $\vec{g} = \text{magnetic charge exists}$

$$\Rightarrow \vec{V} \cdot \vec{B} = \mu_0 \rho_m$$

b/c $\vec{V} \perp (\vec{V} \times \vec{E})$

$$\Rightarrow \vec{V} \cdot (\vec{V} \times \vec{E}) = - \frac{\partial}{\partial t} (\vec{V} \cdot \vec{B}) = 0$$

but $\vec{V} \cdot \vec{B} = \mu_0 \rho_m \Rightarrow - \frac{\partial}{\partial t} [\mu_0 \rho_m] = + \vec{V} \cdot \vec{J}_m$

magnetic charge conservation, $\frac{\partial}{\partial t} \rho_m + \vec{V} \cdot \vec{J}_m = 0$ current of magnetic charge

to his Faraday Law \Rightarrow add

$$\vec{V} \times \vec{E} = - \frac{\partial \vec{B}}{\partial t} - \mu_0 \vec{J}_m$$

Maxwell

$$\vec{D} \cdot (\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}) \quad \vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$$

$$0 = -\frac{\partial}{\partial t} \vec{D} \cdot \vec{B} = 0 \quad ; \text{ Faraday's law is valid}$$

$$(6) \quad \vec{D} \cdot (\vec{\nabla} \times \vec{B}) = 0 = \mu_0 \vec{\nabla} \cdot \vec{J} = \mu_0 \left(-\frac{\partial \vec{B}}{\partial t} \right) \neq 0$$

if ρ vanishes

\Rightarrow a fix is needed. → we add ρ to $\mu_0 \vec{\nabla} \cdot \vec{J}$

$$\text{Suppose, } \mu_0 \left[\vec{\nabla} \cdot \vec{J} + \frac{\partial \vec{B}}{\partial t} \right] = 0$$

Gauss's law

$$= \mu_0 \left[\vec{\nabla} \cdot \vec{J} + \epsilon_0 \frac{\partial \vec{E}}{\partial t} \right] = 0$$

$$\mu_0 \vec{\nabla} \cdot \left[\vec{J} + \epsilon_0 \frac{\partial \vec{E}}{\partial t} \right]$$

\curvearrowleft add to Faraday's law

$$\Rightarrow \boxed{\vec{\nabla} \times \vec{B} = \mu_0 \left[\vec{J} + \epsilon_0 \frac{\partial \vec{E}}{\partial t} \right]}$$

displaced current

Correct?

$$\vec{\nabla} \cdot \vec{E} = \rho/\epsilon_0$$

$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\vec{\nabla} \times \vec{B} = \mu_0 \left[\vec{J} + \epsilon_0 \frac{\partial \vec{E}}{\partial t} \right]$$

Take

$$\vec{\nabla} \times (\vec{\nabla} \times \vec{E}) = -\frac{\partial}{\partial t} (\vec{\nabla} \times \vec{B})$$

$$= -\frac{\partial}{\partial t} \left[\mu_0 \vec{J} + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t} \right]$$

o, in free space

$$\vec{\nabla} \left(\vec{\nabla} \cdot \vec{E} \right) - \vec{\nabla}^2 \vec{E} = -\mu_0 \epsilon_0 \frac{\partial^2 \vec{E}}{\partial t^2}$$

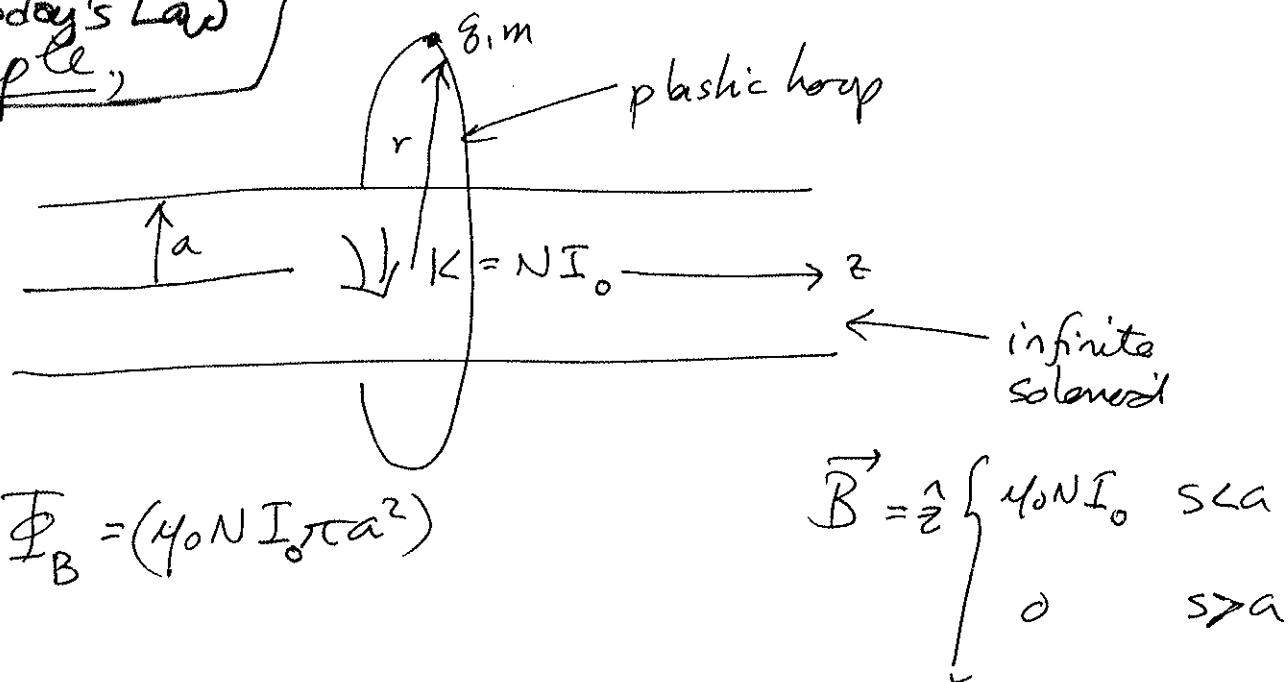
/ ϵ_0

$$\Rightarrow \vec{\nabla}^2 \vec{E} - \mu_0 \epsilon_0 \frac{\partial^2 \vec{E}}{\partial t^2} = 0$$

(and a similar wave equation for \vec{B})

$\mu_0 \epsilon_0 = \frac{1}{c^2} \Rightarrow$ EM radiation is "light"
(or vice versa)

Faraday's Law Example



Turn off current

$$(i) \oint \vec{E} \cdot d\vec{l} = - \frac{d\Phi_B}{dt} = -\mu_0 N \pi a^2 \frac{dI}{dt} = E_\phi / 2\pi r$$

Emf is induced by the changing I

(ii) The torque exerted on γ is

$$\vec{N} = \vec{r} \times \vec{F}$$

$$= rg \vec{E}_\phi \hat{\phi} \quad \text{rotate around } z\text{-axis} \rightarrow$$

$$(i) \& (ii) \Rightarrow |\vec{N}| = rg \left[-\frac{\mu_0 N \pi a^2}{2\pi r} \frac{dI}{dt} \right]$$

$$N = \frac{dL}{dt} = -g \left(\frac{\mu_0 N a^2}{2} \right) \frac{dI}{dt}$$

integrate over time,

$$L = -\frac{1}{2} (\mu_0 N a^2 g) [I(\infty) - I(0)]$$

$$= \frac{1}{2} \mu_0 N I_0 a^2 g$$

a) steady-state
b) int. states as initial $\xrightarrow{\text{steady-state}}$

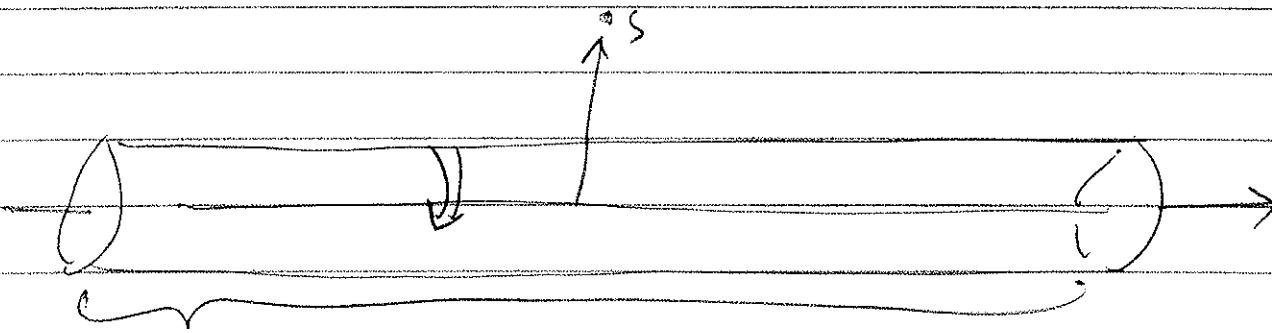
$$L = \vec{r} \times \vec{p} / m = m r v_f = \frac{1}{2} \mu_0 N I_0 a^2$$

$$v_f = \frac{1}{2} \frac{\mu_0 N I_0 a^2}{m r}$$

We made an assumption here. Took the idea that I changed instantaneously. This, strictly speaking, is not correct. This is referred to as the

"quasi-static approximation"

When does this break down?



For a finite solenoid, by the L , the field at its center axis is

$$B_z = \frac{\mu_0 N I L}{2 \sqrt{R^2 + (L/4)^2}}$$

For an infinite solenoid,

$$B_z^{\infty} = \mu_0 N I$$

so, to be arbitrary, let's say that if $L \geq L_0$,

$$B_z \geq 0.9 B_z^{\infty}$$

$$\frac{B_z}{B_{z\infty}} = \frac{\frac{\mu_0}{2} N \times L}{\sqrt{R^2 + \frac{L^2}{4}}} \approx \frac{L}{2\sqrt{R^2 + \frac{L^2}{4}}} = 0.9$$

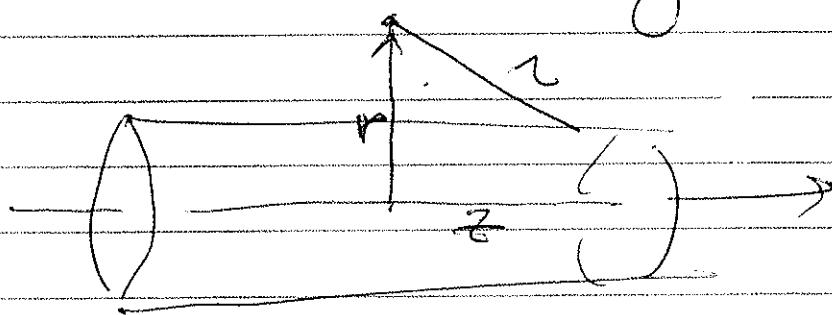
$$\Rightarrow \frac{L^2}{4} = 0.9^2 \left(R^2 + \frac{L^2}{4} \right)$$

$$0.19 \left(\frac{L^2}{4} \right) = 0.81 R^2$$

$$\Rightarrow \left(\frac{L}{R} \right)^2 \approx 4$$

If the length, L , is roughly, $4 \times R$, then the field is $\sim 90\%$ of the infinite solenoid.

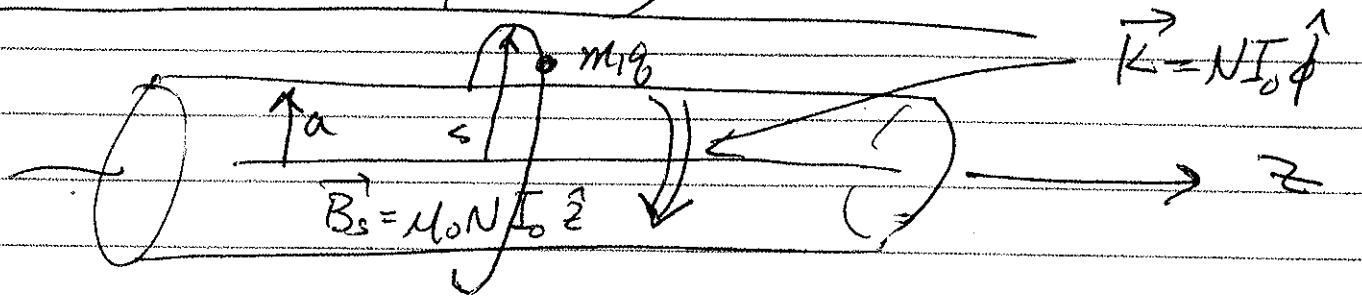
So, as long as the gap between center & $L \approx 4R$ is small, then the field is quasi-static.



$$T = \frac{r}{c} - \frac{r}{c} \approx \frac{\sqrt{r^2 + z^2}}{c} \approx \frac{r}{c} \approx \frac{2}{c} \frac{r}{r + \frac{r^2}{2c}}$$

If $T \ll$ the one while I chose, then we're good.

Consider the same problem, but use \vec{A}



a) what is \vec{A} outside of the solenoid?

$$\vec{B} = \vec{\nabla} \times \vec{A} \Rightarrow \int \vec{B} \cdot d\vec{s} = \int (\vec{\nabla} \times \vec{A}) \cdot d\vec{s}^2$$

$\uparrow = \oint \vec{A} \cdot d\vec{l}$

and so,

$$\mu_0 N I \pi a^2 = A_\phi 2\pi s$$

$$\Rightarrow \vec{A}_\phi = \frac{\mu_0 N I a^2}{2s} \hat{\phi}$$

b) Cut the current $\Rightarrow I \rightarrow 0 \Rightarrow A_\phi \rightarrow 0 \rightarrow E$

$$E = \oint \vec{E} \cdot d\vec{l} = - \frac{d\Phi_B}{dt}$$

$$= - \frac{d}{dt} \int \vec{B} \cdot d\vec{s}$$

but

$$= - \frac{d}{dt} \oint \vec{A} \cdot d\vec{l}$$

$$\Rightarrow E_{\phi} 2\pi s = - \frac{d}{dt} (A_\phi 2\pi s)$$

$$\text{and so } \boxed{E_f = -\frac{dA_f}{dt}} \quad (\text{see next page})^*$$

c) $m(\dot{\phi}) = g E_f$

$$= g \frac{d}{dt} \left(\frac{\mu_0 N I_0 a^2}{2s} \right)$$

Integrate over time \int_0^∞

$$m \dot{\phi} \Big|_0^\infty = - \frac{\mu_0 N a^2}{2s} \left(I(\infty) - I_0 \right)$$

$$m V_f = \frac{\mu_0 N a^2}{2s} I_0$$

$$\boxed{V_f = \frac{g}{m} \left(\frac{\mu_0 a^2 N I_0}{2s} \right)}$$

Comment

(i) $\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$; Faraday's law

if $\frac{\partial \vec{B}}{\partial t} = 0 \Rightarrow \vec{\nabla} \times \vec{E} = 0$ ad

$\vec{E} = -\vec{\nabla} V$, but

$\vec{\nabla} \times \vec{E} \neq 0$, so what's up?

(ii) $\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$. Well $\vec{\nabla} \cdot \vec{B} = 0$ (still)
 $\Rightarrow \vec{B} = \vec{\nabla} \times \vec{A}$ is

still true

$$= -\frac{\partial}{\partial t} (\vec{\nabla} \times \vec{A})$$

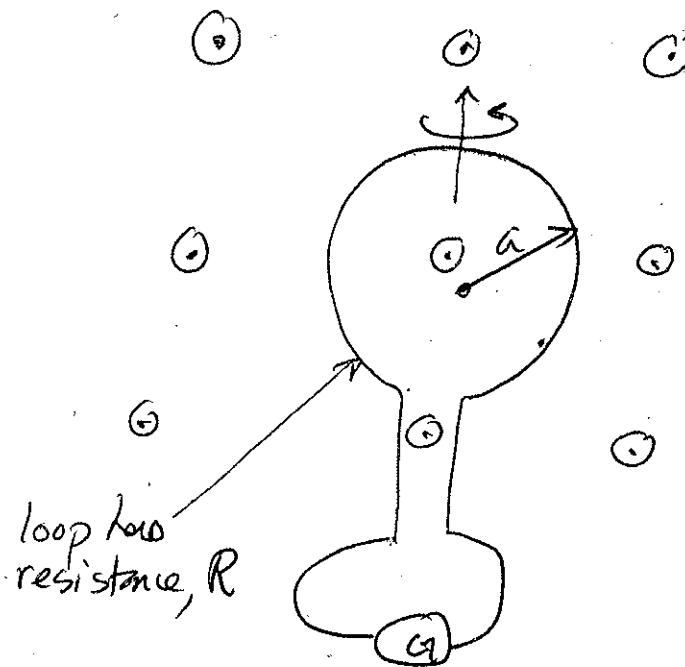
$$\Rightarrow \vec{\nabla} \times \left[\vec{E} + \frac{\partial \vec{A}}{\partial t} \right] = 0 \text{ is true } \checkmark \text{ so far fine (again)}$$

$$\Rightarrow \vec{E} + \underbrace{\frac{\partial \vec{A}}{\partial t}}_{\text{ad}} = -\vec{\nabla} V$$

$$\text{ad } \boxed{\vec{E} = -\vec{\nabla} V - \frac{\partial \vec{A}}{\partial t}}$$

Device to Measure \vec{B}

Flux Coil (measurement of \vec{B})



a) loop sits in plane of paper col \vec{B} is normal to the paper.

b) coil is then rotated 180° regarding the flux through the loop as Φ_B changes, we see an

$$\mathcal{E} = -\frac{d\Phi_B}{dt}$$

at the galvanometer.

So,

$$\mathcal{E} = -\frac{d\Phi_B}{dt}$$

$$= +IR \quad \left. \begin{array}{l} \text{Voltage drop across loop of resistance} \\ R \end{array} \right\}$$

$$= R \frac{dQ(t)}{dt} \quad \left. \begin{array}{l} \text{charge (watchdog) that has flowed through the Galvanometer} \\ \text{at time } t. \end{array} \right\}$$

$$\Rightarrow R \frac{dQ}{dt} = -\frac{d}{dt} \Phi_B$$

Integrate over time from $t=0 \rightarrow \infty$

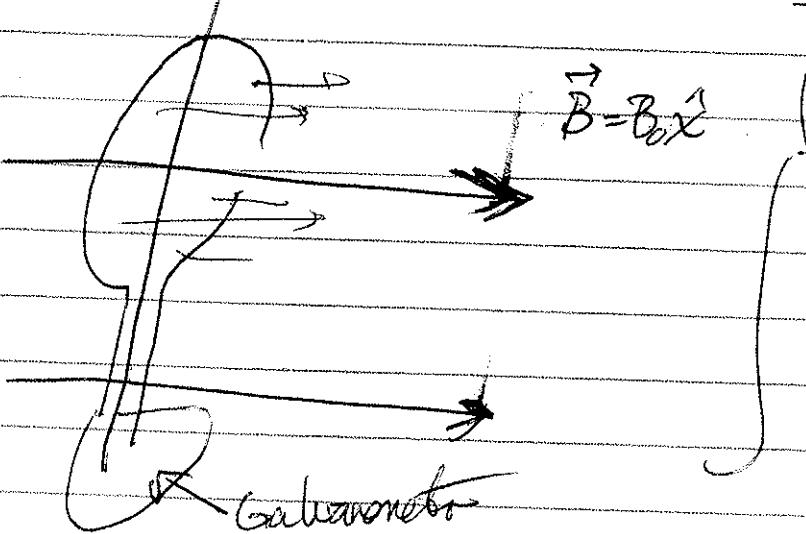
$$R[Q(\infty) - Q(0)] = -\Phi_B(\infty) + \Phi_B(0)$$

$$RQ(\infty) = +\pi a^2 B + \pi a^2 B$$

$$\Rightarrow \boxed{B = \frac{RQ}{2\pi a^2}} \quad \left. \begin{array}{l} \text{Solve } \vec{B} \text{ for} \\ \text{residual of } Q \end{array} \right\}$$

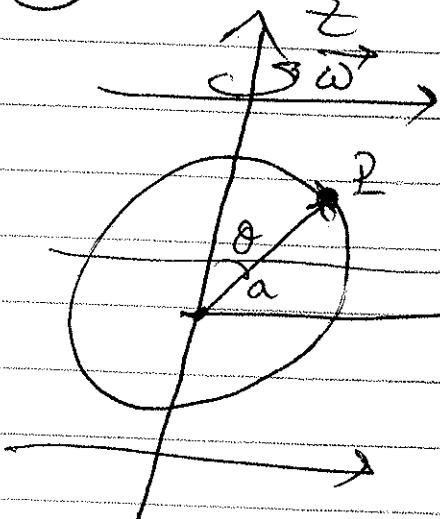
Reso the flip coil using Lorentz force law

$$\vec{\omega} = \omega_0 \hat{z} = \dot{\phi} \hat{z}$$



We will solve
 $E = \oint \vec{B} \cdot d\vec{l}$
 around coil at a given
 time $t \Rightarrow \phi(t)$) and
 then find $\int E(t) dt$
 to get flow of charge

a) Side view let coil lie in x-z plane



$$\text{Point P has coordinates } \vec{r}_P = (a \sin \theta \cos \phi, a \sin \theta \sin \phi, a \cos \theta)$$

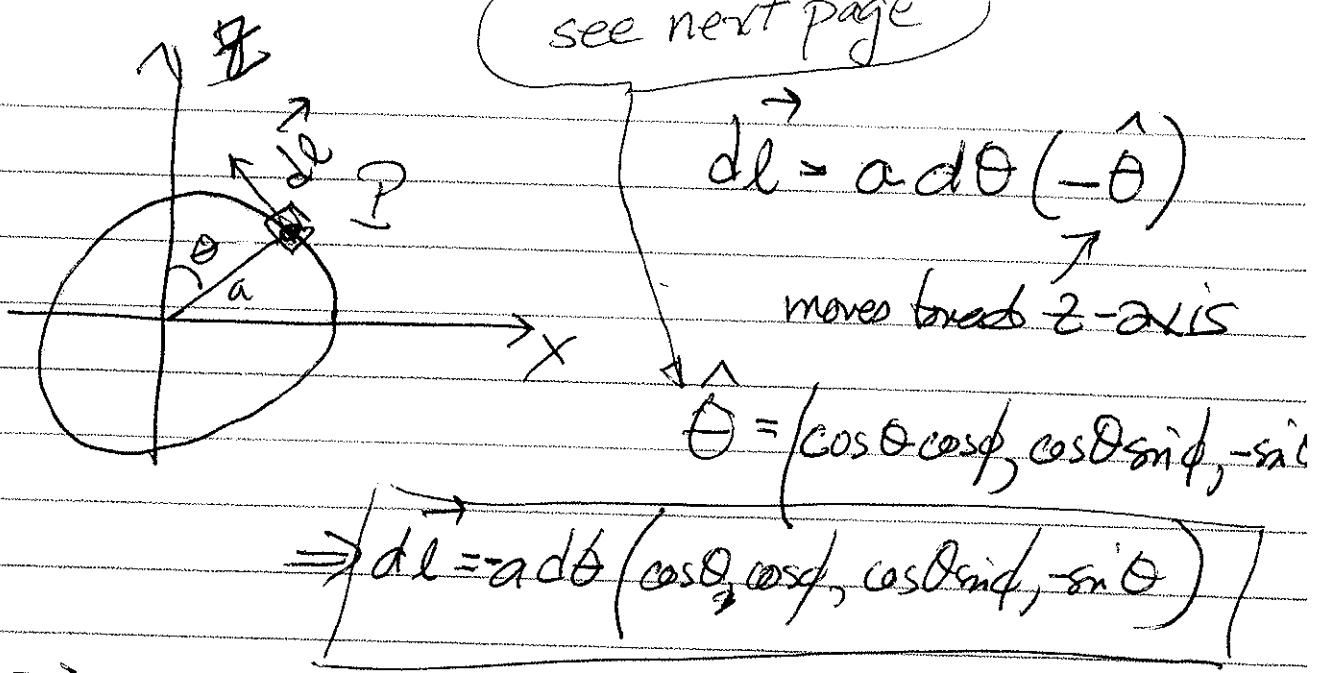
$$\vec{\omega} = (0, 0, \omega_0)$$

$$\vec{V}_P = \vec{\omega} \times \vec{r}_P$$

$$= (-\omega_0 a \sin \theta \sin \phi, \omega_0 a \sin \theta \cos \phi, 0)$$

$$\vec{F}_P = \vec{V}_P \times \vec{B} = (-\omega_0 a \sin \theta \sin \phi, \omega_0 a \sin \theta \cos \phi, 0) \times (B_0, 0, 0)$$

$$= (0, 0, -\omega_0 a \sin \theta \cos \phi B_0)$$



$$\begin{aligned} \vec{f} \cdot \vec{dl} &= (0, 0, -\omega_0 a \sin \theta \cos \phi) \cdot (-a d\theta) (\cos \theta \cos \phi, \cos \theta \sin \phi, -\sin \theta) \\ &= -a d\theta \omega_0 a B_0 (0, 0, \sin^2 \theta \cos \phi) \end{aligned}$$

$$E = \oint \vec{f} \cdot \vec{dl}$$

$$= -\omega_0 a^2 B_0 \int \sin^2 \theta \cos \phi d\theta$$

$$= -\omega_0 a^2 B_0 \pi \cos \phi$$

$$(E = -(B_0 \pi a^2) \dot{\phi} \cos \phi)$$

$$\dot{\phi} = \frac{d\phi}{dt}$$

now,

$$E = IR = R \frac{dQ}{dt} = -B_0 \pi a^2 \dot{\phi} \cos \phi$$

Integrate for $t=0$ when $\dot{\phi} = \frac{\pi}{2}$ to

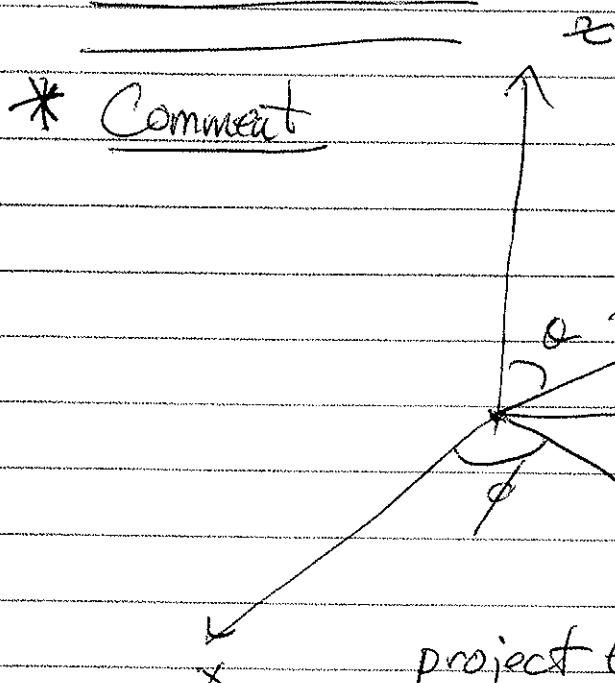
$$t = \infty \text{ when } \dot{\phi} = \frac{3\pi}{2}$$

$$\Rightarrow R [Q(\infty) - Q(0)] = -B_0 \pi a^2 \left[\sin\left(\frac{3\pi}{2}\right) - \sin\left(\frac{\pi}{2}\right) \right]$$

$$\Rightarrow RQ(\alpha) = B_0 \pi a^2 2$$

$$B_0 = \frac{RQ(\alpha)}{2\pi a^2}$$

as before



$$\begin{aligned} \hat{r} = & \sin \theta \cos \phi \hat{x} \\ & + \sin \theta \sin \phi \hat{y} \\ & + \cos \theta \hat{z} \end{aligned}$$

what is $\hat{\theta}$?

$$\frac{\pi}{2} - \theta = \psi$$

project $\hat{\theta}$ onto x-y plane and take $(\cos \psi, \sin \psi)$

$$\begin{aligned} \hat{\theta} = & \sin\left(\frac{\pi}{2} - \theta\right) \cos \psi \hat{x} + \sin\left(\frac{\pi}{2} - \theta\right) \sin \psi \hat{y} \\ & + \cos\left(\frac{\pi}{2} - \theta\right) \hat{z} \end{aligned}$$

$$\hat{\theta} = \cos \theta \cos \phi \hat{x} + \cos \theta \sin \phi \hat{y} - \sin \theta \hat{z}$$

This is good, Inductance

Hum, but we ignored induced currents (and the induced fields). Is this okay?

Let's see, if we change I by $dI \Rightarrow$ we get some dI

Suppose we write,

$$\text{Inductance} \Rightarrow d\Phi_B^{\text{ind}} \propto dI = L dI$$

Self-inductance (return to this later)

We then have,

$$d\Phi_B = d\Phi_B^c + d\Phi_B^{\text{ind}}$$

$$= d\Phi_B^c + L dI$$

$$E = -\frac{d\Phi_B}{dt} = -\frac{d\Phi_B^c}{dt} - L \frac{dI}{dt} = R \frac{dQ}{dt}$$

integrate over time

$$-\left(\Phi_B(\infty) - \Phi_B(0)\right) - L \left(I(\infty) - I(0)\right)$$

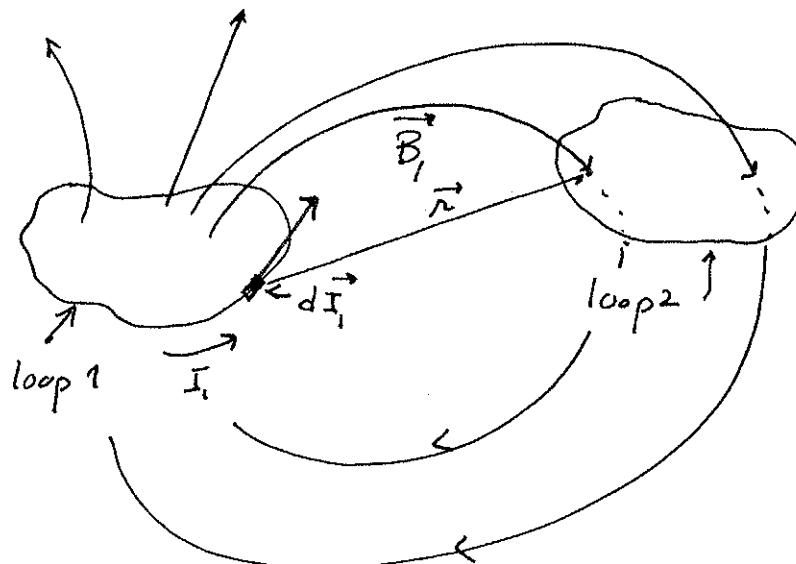
$$= R(Q[\infty] - Q[0])$$

and we get the same result. Self-inductance affects how the system changes, but once at its steady-state, it goes away.

Let's look at inductance in more detail

Inductance

When talking about generators, we had to consider back emf's, i.e., E arises around a coil which generates a \vec{B}_B opposite to the slope in $\Phi_{B,\text{original}}$. We introduced inductance to account for back emf.



$$(i) \vec{B}_1 = \frac{\mu_0}{4\pi} \vec{I}_1 \times \hat{r} \Rightarrow \Phi_2 = \int \vec{B}_1 \cdot d\vec{s}_2$$

$$\vec{B}_1 \propto \vec{I}_1 \Rightarrow \Phi_2 \propto I_1 \text{, ad we define}$$

$$\Phi_2 = M_{21} I_1$$

~ mutual inductance

(ii) M_{21} seems complex, but let's consider some manipulations of M_{21} .

Show that $M_{21} = M_{12}$

$$\Phi_2 = \int \vec{B}_1 \cdot d\vec{S}_2 \\ = \int (\vec{\nabla} \times \vec{A}_1) \cdot d\vec{S}_2$$

Stokes's theorem

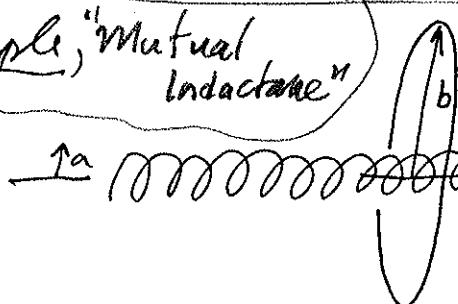
$$\rightarrow \Phi_2 = \oint \vec{A}_1 \cdot d\vec{l}_2 \\ = \oint \left[\frac{\mu_0}{4\pi} \oint \frac{I_1 d\vec{l}_1}{r} \right] \cdot d\vec{l}_2 \\ = \frac{\mu_0 I_1}{4\pi} \oint \oint \frac{d\vec{l}_1 \cdot d\vec{l}_2}{r}$$

Neumann formula

$$\Rightarrow M_{21} = \frac{\mu_0}{4\pi} \oint \oint \frac{d\vec{l}_1 \cdot d\vec{l}_2}{r} \quad \text{is symmetric in "1" and "2"}$$

$$\Rightarrow M_{21} = M_{12} ! \quad \text{Mutual Inductance}$$

Example, "Mutual Inductance"



1a \leftarrow Infinite solenoid; (N, I)

Current I flows in the loop, what is the Φ_B through the solenoid?

$$\Phi_{\text{Sol}} = M_{\text{sol,loop}} I_{\text{loop}}$$

↑ extremely complex

Since \vec{B}_{loop} and
you do \vec{B}_{loop} for
 $d\vec{B}_{\text{loop}} \cdot d\vec{S}_{\text{sol}}$ for
every loop!

\vec{B}_e is difficult and we must integrate flux each turn of the solenoid!

$$\oint \vec{B}_e \cdot d\vec{S}_e = M_{se} I_e$$

b) $\oint \vec{B}_s \cdot d\vec{S}_s \leftarrow \text{Use symmetry}$

$$= \mu_0 N I_s \pi a^2 \Rightarrow \oint \vec{B}_s \cdot d\vec{S}_s = M_{es} I_s (+)$$

$M_{es} = \mu_0 N \pi a^2 = M_{es}$

take advantage of the fact that

$$M_{21} = M_{12}$$

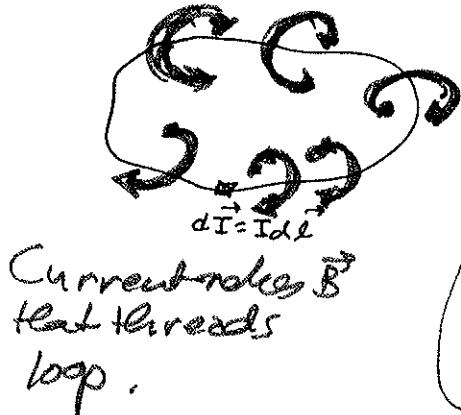
and use the flux link loop to find $M_{sol,loop}$

$$= \oint \vec{B}_s \cdot d\vec{S}_{loop}$$

to get $M_{sol,loop}$ and then $M_{loop,sol}$

$$\Rightarrow \oint \vec{B}_s \cdot d\vec{S}_{loop} = (\mu_0 N) \pi a^2 I_{loop}$$

Self-Inductance



If I varies $\Rightarrow \vec{B}_s$ then loop varies

$\Rightarrow E$ opposes change in set-up

\Rightarrow Self-induction

$$d\vec{\Phi} = L dI$$

$$\Rightarrow E = -L \frac{dI}{dt}$$

In practice, this is a difficult proposition.

infinite solenoid
w/ I and N

and $\oint \vec{B}_s \cdot d\vec{S}_z = \underbrace{(\mu_0 N I_a \pi a^2)}_{\text{flux thru 1 loop}} \times \underbrace{Ndz}_{\# \text{ of loops mid } z}$

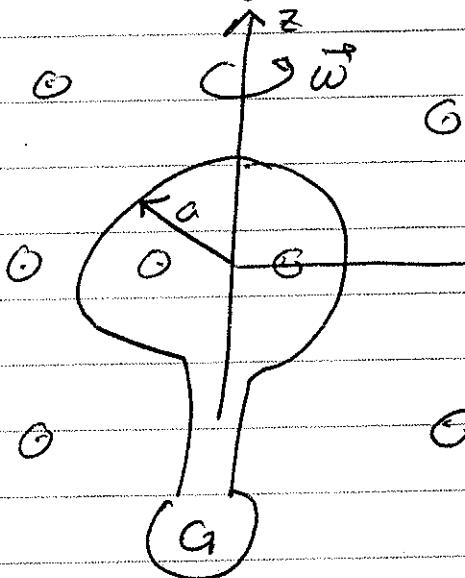
$$\Rightarrow \vec{B} = \mu_0 N I_a \hat{z}$$

$$\oint_B \Phi = \mu_0 I \pi a^2 N^2 \overbrace{l_z}^1 = L I$$

some length
 l_z

$$\Rightarrow L = (\mu_0 N^2 \pi a^2) \equiv \text{inductance per unit length}$$

Alternating Current (AC) Generator



θ

$$\omega \vec{\omega} = \omega_0 \hat{z}$$

θ

θ

θ

$$a) \vec{B} = B_0 \hat{x}$$

Set-up the problem

$$a) E_s = ?$$

E

$$a) E = \oint \vec{f} \cdot d\vec{l} = - \frac{d\Phi}{dt}$$

$$E_F = - \frac{d\Phi_B^C}{dt}, E_L = - \left[L \frac{dI}{dt} \right], E_R = - IR$$

no di/dt voltage

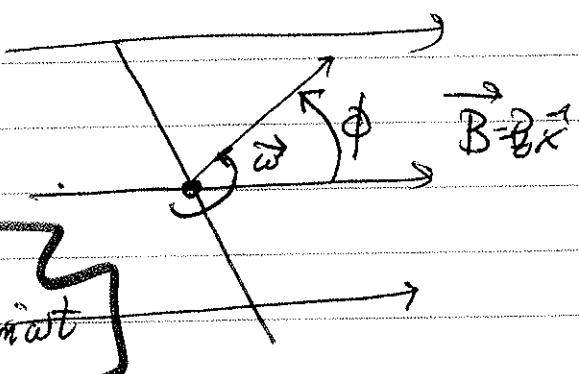
$$\Rightarrow O = E_F + E_L + E_R$$

So $E_F = - \frac{d\Phi_B^C}{dt}$

$\vec{\Phi}_B$

$$\vec{\Phi}_B = (B_0 \pi a^2) \cos \phi$$

$$= \Phi_0 \cos(\omega t) \Rightarrow \frac{d\Phi}{dt} = -\omega \Phi_0 \sin(\omega t)$$



$$\text{Solve } L \frac{dI}{dt} + RI = w \int_0^t \sin \omega t \, dt$$

$\overbrace{-E_L}^{\text{in}}$ $\overbrace{-E_R}^{\text{in}}$ $\overbrace{E_F}^{\text{out}}$ } $\text{from } O = E_F + E_R$

Solve the homogeneous part ($= 0$) and then
the particular part ('steady-state')

a) Homogeneous

$$L \frac{dI}{dt} + RI = 0 \Rightarrow \frac{1}{I} \frac{dI}{dt} = -\frac{R}{L}$$

$$\ln I / \underbrace{I(0)}_{= R/L} = -\frac{R(t-0)}{L}$$

$$I = I_0 e^{-\frac{Rt}{L}}$$

b) Particular (Steady-state)

$$L \frac{dI}{dt} + RI = w \int_0^t \sin \omega t \, dt$$

$$\text{Set } I = A \sin(\omega t + \varphi)$$

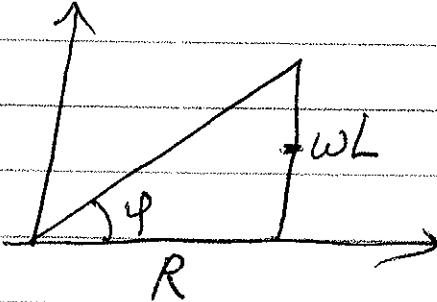
$$\omega L A \cos(\omega t + \varphi) + R A \sin(\omega t + \varphi) = w \int_0^t \sin \omega t \, dt$$

Find φ and A

$$\text{at } t=0, \omega L A \cos(\varphi) + R A \sin(\varphi) = 0$$

$$\Rightarrow \tan \varphi = -\frac{\omega L}{R}$$

$$\text{at } \omega t = \frac{\pi}{2}, \underbrace{\omega L A \cos\left(\frac{\pi}{2} + \varphi\right)}_{-\sin \varphi} + \underbrace{RA \sin\left(\frac{\pi}{2} + \varphi\right)}_{\cos \varphi} = \omega$$



$$\cos \varphi = \frac{R}{\sqrt{\omega^2 L^2 + R^2}}, \sin \varphi = -\frac{\omega L}{\sqrt{\omega^2 L^2 + R^2}}$$

$$\Rightarrow \omega L A \left(\frac{\omega L}{\sqrt{\omega^2 L^2 + R^2}} \right) + RA \left(\frac{R}{\sqrt{R^2 + \omega^2 L^2}} \right) = \omega I_0$$

$$A \left[\sqrt{R^2 + \omega^2 L^2} \right] = \omega I_0 \Rightarrow A = \frac{\omega I_0}{\sqrt{R^2 + \omega^2 L^2}}$$

$$\Rightarrow I(t) = I_0 e^{-Rt/L} + \frac{\omega I_0}{\sqrt{R^2 + \omega^2 L^2}} \sin(\omega t + \varphi)$$

¶

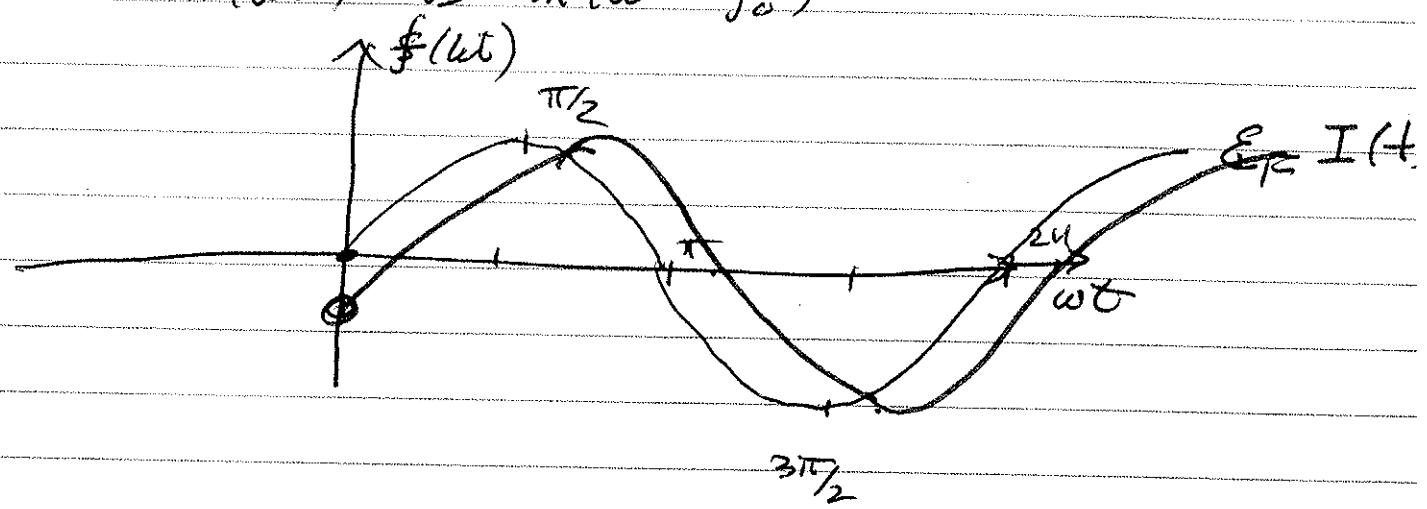
E_F ad $I(t)$ are out of phase

$$\begin{matrix} \nearrow & \swarrow \\ \sin(\omega t) & \sin(\omega t + \varphi) \end{matrix}$$

$$2 \tan \varphi = -\frac{\omega L}{R}$$

\Rightarrow current lags the E_F .

$\sin(\omega t)$ vs $\sin(\omega t - \varphi_0)$



$$\Phi_0 = B\pi a^2$$

$$E = \Phi_0 \omega \sin(\omega t)$$

$$I = \frac{\omega \Phi_0}{R \sqrt{1 + (\frac{\omega L}{R})^2}} \sin\left(\omega t - \tan^{-1} \frac{\omega L}{R}\right)$$

In steady-state

Determine the power output

$$P = IV = I^2 R = \frac{\Phi_0^2 \omega^2}{R^2 \left(1 + \frac{\omega^2 L^2}{R^2}\right)} \sin^2(\omega t - \phi_w) \times R$$

$$\langle P \rangle = \frac{\omega}{2\pi} \int_0^{2\pi/\omega} P dt = \frac{\omega}{2\pi} \int_0^{2\pi/\omega} \frac{\omega^2 B^2 \pi^2 a^4}{R^2 \left(1 + \frac{\omega^2 L^2}{R^2}\right)} \times R \sin^2(\omega t - \phi_w) dt$$

↑
average
over 1
cycle

$$= \frac{\omega^3 B^2 a^4 \pi}{2R \left(1 + \frac{\omega^2 L^2}{R^2}\right)} \int_0^{2\pi/\omega} \sin^2(\omega t - \phi_w) dt$$

$$\text{let } u = \omega t - \phi_w \Rightarrow du = \omega dt$$

$$= \frac{\omega^2 B^2 a^4 \pi}{2R \left(1 + \frac{\omega^2 L^2}{R^2}\right)} \int_{-\phi_w}^{2\pi/\omega - \phi_w} \sin^2 u du$$

$$\boxed{\langle P \rangle = \frac{(\pi \omega B a^2)^2}{2R \left(1 + \frac{\omega^2 L^2}{R^2}\right)}}$$

recall:

$$\boxed{\frac{(\omega B a^2)^2}{4R} = P_{HG}}$$

differs by $\frac{2\pi^2}{(1 + \omega^2 L^2/R^2)}$

Alternatively,

$$L \frac{dI}{dt} + RI = \omega_0^2 \sin \omega t$$

Consider $\tilde{I}(t) = I_0 e^{i\omega t}$, ad dly force $\omega_0^2 e^{i\omega t}$

use $i\omega t$ in eqn. r.h.s
this result

$$i\omega L \tilde{I}_0 e^{i\omega t} + R \tilde{I}_0 e^{i\omega t} = \omega_0^2 \tilde{I}_0 e^{i\omega t}$$

(i) Solve homogeneous equation

$$\left[i\omega L \tilde{I}_0 + R \tilde{I}_0 \right] = 0$$

$$\tilde{I}_0 [i\omega L + R] \Rightarrow i\omega L = -R, \omega = -\frac{R}{iL} = \omega_L$$

ad $\tilde{I}_h(t) = \tilde{I}_0 e^{-\omega_L t}$ \rightarrow damping transient

(ii) Solve particular solution

$$i\omega L \tilde{I}_0 + R \tilde{I}_0 = \omega_0^2 \tilde{I}_0$$

$$\tilde{I}_0 = \frac{\omega_0^2 \tilde{I}_0}{i\omega L + R} = \frac{\omega_0^2 \tilde{I}_0}{(\omega L)^2 + R^2} (R - i\omega L)$$

$$\Rightarrow I_{0,R} = \frac{\omega_0^2 R}{(\omega L)^2 + R^2}, I_{0,I} = -\frac{\omega_0^2 L \tilde{I}_0}{(\omega L)^2 + R^2}$$

$$\Rightarrow \tilde{I}_0 = I_{0,R} + i I_{0,I} = \sqrt{I_{0,R}^2 + I_{0,I}^2} e^{i \tan^{-1}\left(\frac{I_{0,I}}{I_{0,R}}\right)}$$

and our sol^{1/2} becomes

$$\tilde{I}(t) = \sqrt{I_{0,R}^2 + I_{0,I}^2} e^{i(wt + \tan^{-1}\frac{I_{0,I}}{I_{0,R}})}$$

we want imaginary part of solution

$$\Rightarrow I(t) = \sqrt{\frac{(\omega I_0 R)^2}{[(\omega L)^2 + R^2]^2} + \frac{(\omega^2 I_0 L)^2}{[(\omega L)^2 + R^2]^2}} \sin\left(wt + \tan^{-1}\left(-\frac{\omega L}{R}\right)\right)$$

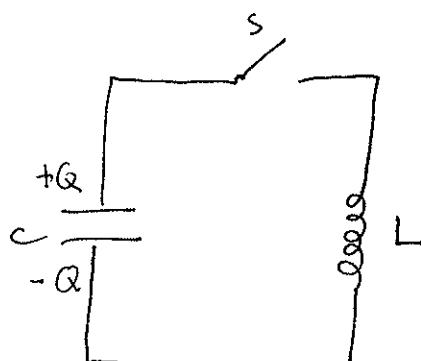
$$I(t) = \frac{(\omega I_0)}{\sqrt{(\omega L)^2 + R^2}} \sin\left(wt - \tan^{-1}\left[\frac{\omega L}{R}\right]\right)$$

(HW)

Prob 7.25

RLC Circuits

C is charged to V and then
S is closed connecting C to
an inductor w/L.



Determine $I(t)$

$$E_L = -\underbrace{\frac{d\Phi_B}{dt}}_{I_B} = -\frac{d}{dt}(LI)$$

as $Q \downarrow, I \uparrow$

$$(i) \boxed{C = Q/V, E_L = -L \frac{dI}{dt} \text{ and } V + E_L = 0}$$

$$\Rightarrow -L \frac{dI}{dt} + \frac{Q}{C} = 0 \rightarrow L \frac{d^2Q}{dt^2} + \frac{Q}{C} = 0, I = -\frac{dQ}{dt}$$

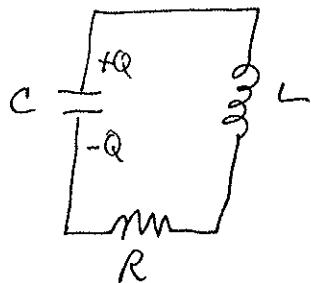
$$\text{Let } Q = Q_0 e^{at} \Rightarrow La^2 Q + \frac{1}{C} Q = 0 \Rightarrow a = \pm i\sqrt{\frac{1}{LC}}$$

$$\text{and } Q = Q_0 \exp\left(\pm i\sqrt{\frac{1}{LC}}t\right)$$

for finite charge

$$\Rightarrow \boxed{I(t) = +Q_0 \sqrt{\frac{1}{LC}} \exp\left(i\sqrt{\frac{1}{LC}}t\right)} \rightarrow \text{current oscillates}$$

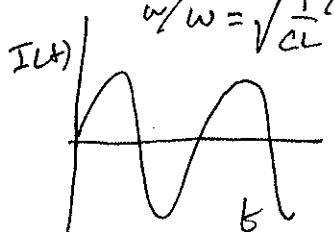
Suppose we add a resistor, R



the voltage drop and the
circuit must be 0

$$\Rightarrow \frac{Q}{C} - L \frac{dI}{dt} - IR = 0, I = -\frac{dQ}{dt}, \text{ as } Q \downarrow, I \uparrow$$

$$L \frac{d^2Q}{dt^2} + R \frac{dQ}{dt} + \frac{1}{C} Q = 0$$



$$\text{Let: } Q = Ae^{at}$$

$$La^2 Q + Ra Q + \frac{1}{C} Q = 0$$

$$\Rightarrow a^2 + \frac{R}{L} a + \frac{1}{LC} = 0 \Rightarrow a = \frac{-\frac{R}{L} \pm \sqrt{\frac{R^2}{L^2} - \frac{4}{LC}}}{2}$$

$$= -\frac{R}{2L} \left(1 \mp \sqrt{1 - \frac{4L}{RC}} \right)$$

for physical solution, $a = -\frac{R}{2L} - \frac{R}{2L} \sqrt{1 - \frac{4L}{RC}}$

$$I(f) = -\frac{dQ}{dt}$$

$$= Q_0 \frac{R}{2L} \left(1 + \sqrt{1 - \frac{4L}{RC}} \right) \exp \left(-\frac{R}{2L} \left[1 + \sqrt{1 - \frac{4L}{RC}} \right] t \right)$$